AIR LEAKAGE OF US HOMES

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ABSTRACT

Air tightness is an important property of building envelopes. It is a key factor in determining infiltration and related wall-performance properties such as indoor air quality, maintainability and moisture balance. Air leakage in U.S. houses consumes roughly 1/3 of the HVAC energy but provides most of the ventilation used to control IAQ. The Lawrence Berkeley National Laboratory has been gathering residential air leakage data from many sources and now has a database of more than 100,000 raw measurements. This paper uses a model developed from that database in conjunction with publically available data for estimating air leakage as a function of location throughout the US.

1. INTRODUCTION

Air leakage through the building envelope contributes to ventilation, heating and cooling costs and moisture migration. Understanding the magnitude of the leakage in an individual envelope is important in optimizing the HVAC system and in retrofitting. Understanding the magnitude of leakage in the building stock is important for prioritizing both research efforts and conservation measures for policy makers in both the public and private sector.

"Air Tightness" is the property of building envelopes most important to understanding ventilation. It is quantified in a variety of ways all of which typically go under the label of "air leakage". Air tightness is important from a variety of perspectives, but most of them relate to the fact that air tightness is the fundamental building property that impacts infiltration. There are a variety of definitions of infiltration, but fundamentally infiltration is the movement of air through leaks, cracks, or other adventitious openings in the building envelope. The modeling of infiltration (and thus ventilation) requires a measure of air tightness as a starting point. More extensive information on air tightness can be found in Sherman and Chan (2003), who review the state of the art. This information is also part of a broader state of the art review on ventilation compiled by Santamouris and Wouters (2005).

Sherman and Chan (2003) also discuss the topic of metrics, reference pressures and one versus two parameter descriptions in some detail and will not be discussed here. We have chosen to use the metric of Normalized Leakage (NL) as defined by ASHRAE Standard 119 (1988, 2005) as our primary metric to describe air tightness of houses because it removes the influence of house size and height:.

$$NL = 1000 \cdot \frac{ELA}{Area} \cdot \left(N_{story}\right)^{0.3} \quad (1)$$

By such a normalization, this metric allows us to compare the leakiness of different house independent of size.

2. MODELING METHODS

This study consisted of two parts: 1) developing a regression model from the leakage data, and 2) applying that model to existing data of housing stock characteristics to come up with leakage characteristics for the United States housing stock. The regression model is documented in other papers (e.g., McWilliams and Jung (2006)). This paper will focus on the application of that model to predict envelope leakage.

The first step in the prediction is to use the model to calculate the leakage area for each county using publicly available data. Once the leakage area is known, we calculate the airflow through the building envelope for every hour of the year using the LBL model (Sherman, 1980) with hourly temperature and wind speed data. The flow is converted to an air change rate by dividing by the volume of the house, and the air change rate can be related to ventilation effectiveness using the Sherman Wilson model (Sherman and Wilson, 1986)

2.1 Leakage Model

McWilliams and Jung (2006) used the data in the LBL air leakage database to create a predictive model that can be used to estimate the air tightness of a house based on certain physical characteristics. Their model is shown in equation (2) and the values of the parameters are shown in Table 1. The parameters, which are all dimensionless, were determined by regression analysis.

$$NL = NL_{cz} \cdot \phi_{Area}^{size-1} \cdot \phi_{Height}^{N_{story}-1} \cdot \phi_{\varepsilon}^{P_{Eff}} \cdot \phi_{Age}^{Age} \cdot \phi_{Floor}^{P_{Floor}} \cdot \left(\phi_{LI,Age}^{Age} \cdot \phi_{LI,Area}^{size-1} \cdot \phi_{LI}\right)^{P_{LI}} \quad (2)$$

Table 1: Values of Model Parameters

ϕ_{Height}	1.156	ϕ_{Floor}	1.08
ϕ_{ε}	0.598	ϕ_{LI}	2.45
ϕ_{Age}	1.012	$\phi_{\text{LI,Age}}$	0.994
ϕ_{Area}	0.841	$\phi_{\text{LI,Area}}$	0.775
NL_{Alaska}	0.36	NL_{Cold}	0.53
NL_{Humid}	0.35	NL_{Dry}	0.61

All of the "P" parameters (P_{LI}, P_{Floor} and P_{Eff}), can be treated in the model as either the probability of being true or as a fraction of the (large) sample for which it is true. P_{LI} is unity for a low-income house and zero otherwise. P_{Eff} if unity if the house has participated in an energy efficiency program and zero otherwise. P_{Floor} is unity if the house has any air leakage through the floor plane and zero if there is no air leakage through that pathway.

The Normalized Leakage coefficients for the four climate zones, NL_{cz}, represent the average normalized leakage for a house in the reference condition. The reference condition is when all of the exponents are zero, which means a 100 m^2, single-story, non-energy efficient, unaged, slab-on-grade, non-low-income house.

The climate zones are based on combinations of those defined by Building Science Corporation as shown in Figure 1 The climates that were used in the model were Humid (made up of Mixed-Humid and Hot-Humid), Dry (made up of Marine, Mixed-Dry and Hot-Dry), Alaska (containing all counties in Alaska), and Cold (all counties in Cold, Very Cold and Subarctic that are not in Alaska). The climate coefficients for Humid and Alaska are similar and substantially lower than the coefficients for the Dry and Cold areas.

Figure 1: Climate Zones

This model is based on a limited dataset, but should provide accurate leakage estimates when applied to broad enough spectrum of houses. Although the uncertainty of an individual prediction is estimated to be on the order of 50%, larger biases may be present when the narrow samples are used. For example, this model is expected to be biased high for conventional new construction, because of increasing improvements made to envelope air tightness in recent years.

2.2Ventilation Model

The LBL ventilation model, shown in Equations (3) thropugh (8), estimates flow through the building shell, Q(t), based on the leakage area of the shell, wind and stack factors, and TMY weather conditions at the house site. The ventilation was calculated for each hour in a typical meteorological year.

$$Q(t) = (ELA) \cdot s(t) \tag{3}$$

where

$$s(t) = \sqrt{f_s^2 \cdot \Delta T + f_w^2 \cdot v^2} \tag{4}$$

$$f_s = \left(\frac{1 + \frac{R}{2}}{3} \right) \left(1 - \frac{x^2}{2 - R^2} \right)^{3/2} \left(\frac{g \cdot h}{T_o} \right)^{1/2} \tag{5}$$

$$f_w = C(1-R)^{1/3} A \left(\frac{h}{10} \right)^B \tag{6}$$

$$X = \frac{A_C - A_F}{A_o} \tag{7}$$

$$R = \frac{A_C + A_F}{A_o} \tag{8}$$

2.3 Stochastic Method

A stochastic simulation method was used in the predictive calculation to produce a distribution of calculated building properties using input distributions of floor area, height, age, foundation type, energy efficiency improvements, and resident income for houses in each of the 3141 United States counties. The stochastic simulation allows the estimation of the mean and standard distribution for each of the calculated properties, namely equivalent leakage area (ELA), and the wind and stack parameters, fw and fs respectively.

For each county, we simulated data for 2000 houses by drawing each of the variables independently from a known distribution for that county. The sample size of 2000 was determined to be sufficient because the distribution did not become better defined when a sample twice as large was used. NL was calculated for each simulated house, and was then transformed into ELA since this is the input variable that is needed to calculate ventilation air flow, Q, in the ventilation model.

2.4 Ventilation Effectiveness

Because ventilation removes pollutants from indoor air, a measure of indoor air quality could be the temporal average of the instantaneous ventilation rate. However, since pollutant concentration is non-linear with respect to ventilation rate a simple average cannot be used. Instead, the term effective ventilation is defined as the steady state ventilation that would yield the same average pollutant concentration over some time period as the actual time varying ventilation in that same time period. It is important to note that the contaminant source strength must be constant over the period of interest. This holds for many building contaminants where the source emission varies slowly with time or operates in a stepwise fashion, and is unaffected by ventilation rate. Some important exceptions are radon, formaldehyde, and carbon monoxide where the emission rate can be affected by the ventilation of the building. In such cases, more detailed techniques may be required.

Effective ventilation is often calculated by first calculating the inverse, the characteristic time for the pollutant concentration to reach steady state, which is given by Equation (9).

$$\tau_{e,i} = \frac{1 - e^{-I_i \Delta t}}{I_i} + \tau_{e,i-1} \cdot e^{-I_i \Delta t} \tag{9}$$

The mean ventilation efficiency is a non-dimensional quantity which is defined as the ratio of the mean effective ventilation to the mean instantaneous ventilation. It is shown in terms of the characteristic time in Equation (10). The closer the actual ventilation rate is to steady state over the period of interest the higher the ventilation efficiency will be.

$$\varepsilon_m = \frac{1}{\overline{I} \cdot \overline{\tau_e}} \qquad (10)$$

3. CHARACTERISTICS

The data used for this project came from several different sources. The house characteristics gathered from publicly available data are: location, floor area, age, height of the structure, whether the house participated in an energy efficiency program, the existence of leakage at the floor level, and the income status of the residents. Sherman and McWillimas (2007) using the detailed work of McWilliams and Jung (2006) have summarized the data sources and the origin of the house characteristics. This information will be summarized, but the reader may refer to the original works for more detail. In the figures below we will examine the variation in specific stock characteristics on a regional or county-by-county basis.

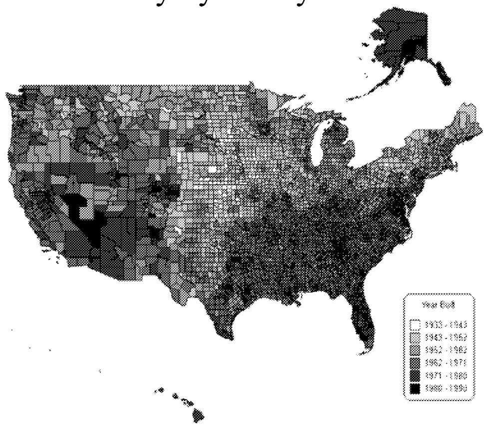

Figure 2: Average Year Built by County

Figure 2 displays the age distribution data and shows that houses in the Northeast and Midwest were built prior to 1950 for the most part, while houses in the Southeast and Southwest were mostly built after 1960.

Each county is represented by a single value, which is the best estimate of the mean for that county. There is, of course, a distribution around this mean in the stock, but we addressing the distribution of each variable in each country was beyond the scope of this study. Regional variation, however, can sometime be inferred by the county-to-county variation.

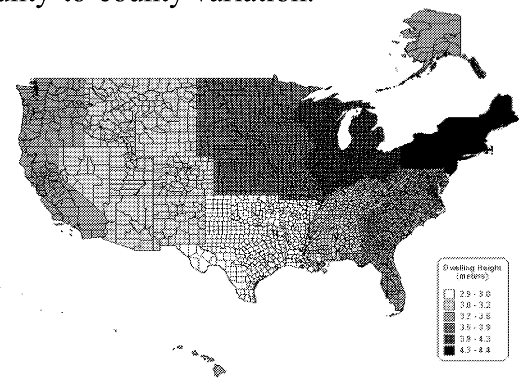

Figure 2: Mean Dwelling Height in Meters by County

Figure 2 and Figure 3, show dwelling height and the probability of floor leaks respectively. The Northeast and Midwest have the tallest dwellings whereas the shortest dwellings are located in the south and west.

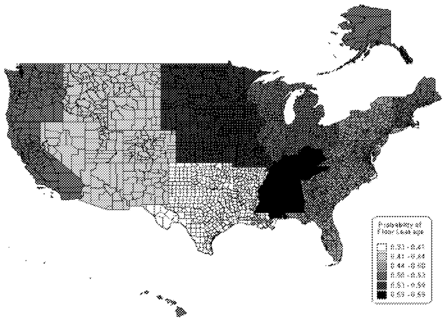

Figure 3: Probability of Floor Leakage by County

The probability of floor leakage is based on foundation type, which is given in three categories: basement, crawlspace or slab on grade. Slab on grade foundations are assigned a leakage probability of 0 because there are no leakage pathways through the slab. Crawlspace foundations were assigned a leakage probability of 1 because there are numerous leakage pathways through penetrations in the floor so we can be fairly sure that there will be some air leakage through these pathways. Conditioned basements, like slab on grade foundations, are assigned a leakage value of 0.

Unconditioned basements, like crawlspaces, are assigned a leakage value of 1.

The mean probability was calculated in each county, and is shown in Figure 3. The highest probability of floor leakage is found in the region consisting of Mississippi, Alabama, Tenessee and Kentucky showing that crawlspace foundations are popular there. The lowest probability of floor leakage is found in the region just next door, containing Texas, Louisiana, Oklahoma and Arkansas where slab on grade foundations are common.

For low-income designation the income threshold was chosen at 125% of the poverty level as per the low-income threshold defined in the Normalized Leakage model developed by McWilliams and Jung (2006). This threshold is the qualification criteria used by the the Ohio Weatherization Program, which provided all of the low-income data used to develop the model.

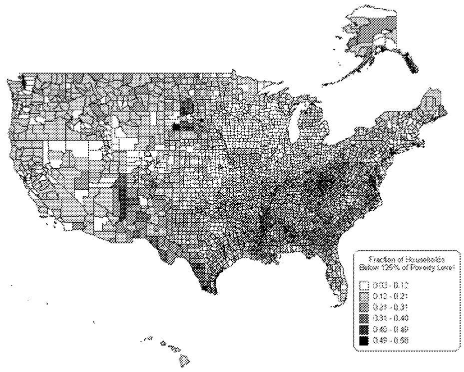

Figure 4: Fraction of Households Below 125% of the Poverty Level by County

Most of the Northeast and Midwest have a low fraction of households below our poverty threshold, as seen in Figure 4. High poverty is concentrated in Appalachia and the South and Southeast, with a few other isolated areas such as central South Dakota, the southern tip of Texas, and one county in eastern Arizona.

The total number of single family dwellings in the United States is 73.7 million. We assumed that 1% of houses nationwide had participated in an energy efficiency program.

Figure 5 shows that larger dwellings are concentrated in the Northeast and Midwest while smaller homes are concentrated in the West and Southwest. The Southeast has larger homes in Mississippi, Alabama and Tenessee and smaller homes from Appalacia to Florida.

The estimate of floor area is a bit weak in some cases. It is unfortunate for such a poorly defined/known parameter that NL has a strong dependence (16% decrease in NL for every 100m^2 increase in floor area) on floor area in the model developed by McWilliams and Jung (2006).

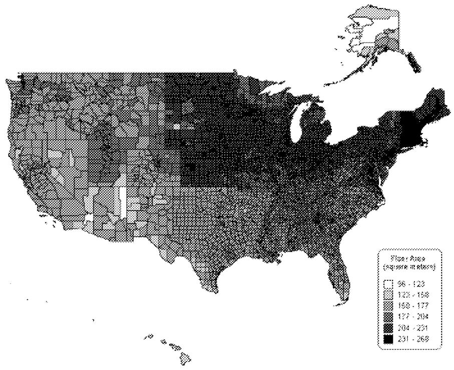

Figure 5: Dwelling Floor Area by County [m^2]

4. RESULTS

The input parameters were used to predict the ventilation for houses in each county. First, the empirical model is used to predict normalized leakage in each county.

Figure 6 shows the normalized leakage across the United States. Immediately visible is the lower normalized leakage in the south east of the country and in Alaska. The boundary of this lower leakage area almost exactly follows the boundary of the humid climate zone. The climate coefficient of 0.35 for the humid climate is similar to the climate coefficient of 0.36 for Alaska. In contrast, the climate coefficients for the cold climate (0.53) and the dry climate (0.61) are much higher.

Another feature of this map that is initially apparent are the two areas of higher normalized leakage, one in northern Louisiana and the other in mid-southern Georgia. These pockets of leaky houses can be attributed to the fact that the houses in these areas are smaller, slightly older, and have a higher percentage of low-income residents than the surrounding counties. Households in Mississippi and Alabama are similar in income, but they are on the order of 50 square meters larger, which decreases NL by 8% according to the model. The higher probability of floor leaks in Mississippi and Alabama increases the NL by 2-3%, which counteracts, but does not negate, the effect of their larger size.

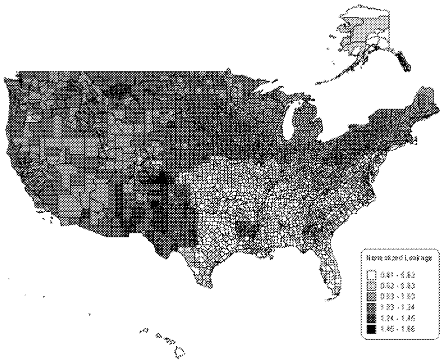

Figure 6: Normalized Leakage by County

The air exchange rate is calculated using the LBL Ventilation model, which predicts flow through the building envelope based on the leakage area of the house and the weather conditions in that location. The shielding class and terrain perameters were both assumed to be moderate, or class III. The leakage distribution parameters, X and R were set according to the floor leakage parameter. Houses with floor leakage were assumed to have one quarter of the leakage in the ceiling, one quarter of the leakage in the floor, and one half in the walls, as in ASHRAE Fundamentals, Chapter 27. Houses with no floor leakage have one third of the leakage in the ceiling and two thirds in the walls. Model predictions are only weakly sensitive to the values of X and R (0-15%, Reinhold and Sonderegger, 1983) so precise determination of these variables is not necessary.

The simulation was performed for each hour over a year of typical weather conditions, and the mean air change rate is shown in

Figure 7. The same pattern can be seen as in Figure 6 with lower air change rate in the tight houses of the Southeast.

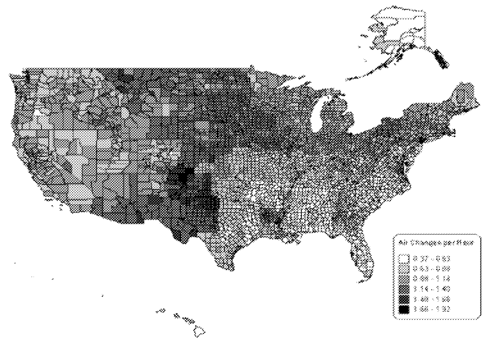

Figure 7: Yearly Average Natural Air Exchange Rate by County

Ventilation efficiency was calculated using the Sherman-Wilson model. It is clearly visible that the milder climates on the west coast and in the south east have ventilation efficiencies closer to 1, indicating that the infiltration is close to steady state over the course of the year. Climates with low ventilation efficiency--as those in the mountainous regions and in the northern part of the country--have increased infiltration variation over the course of the year.

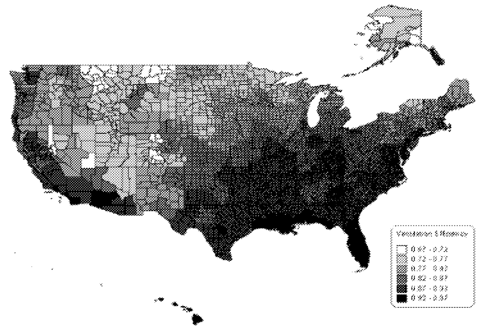

Figure 8: Ventilation Efficiency by County

Effective ventilation shows how much ventilation is going towards reducing exposure for human occupants to pollutants. Figure 9 presents this data in air change rates and shows that Alaska and the Southeast have the lowest effective ventilation.

When effective ventilation is calculated for each month of the year, we find most of the country experiences the highest ventilation rate during the summer months. Some parts of the Midwest and areas on the Gulf of Mexico experience the highest ventilation in the spring, contrastingly the east coast of Florida and Seattle experience the highest ventilation in October. Only the interior of Alaska experiences the highest ventilation rate in the winter, although the maximum effective ventilation values are very similar in Alaska in summer and winter.

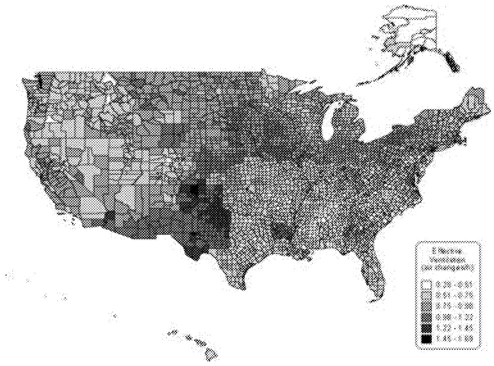

Figure 9: Effective Ventilation by County

5. CONCLUSIONS

This report has presented and used a statistical model for predicting the air tightness of any U.S. home based on location, age, size and configuration. While this model is expected to have an uncertainty of approximately 50% for an individual prediction it can be used on larger populations to predict regional and other trends.

The housing stock in the U. S. contains a negligible number of houses with mechanical ventilation systems therefore infiltration provides the ventilation in these houses. Our results indicate that the vast majority of the residential building stock has effective air change rateas above 0.35 air changer per hour and therefore gets sufficient ventilation from infiltrations when looked at on an annual basis.

Our analysis can help to select which regions may be particularly good candidates for saving energy through air tightening, such as through weatherization programs. The data contained herein has been used to estimate leakage trends, but could, in the future, be used to estimate potential energy savings.

Because there can be a substantial veariation between individual houses, many tighter homes—including most new construction—will likely not be sufficiently ventilated by infiltration alone. In these cases both energy and IAQ gains can be made through a combination of air tightening and designed ventilation systems.

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List of Symbols

Age	Age of house (yr)
Area	floor area inside the pressure boundary (m^2) [ft^2]
ELA	Effective Leakage Area as measured by ASTM E779 or equivalent (m^2) [ft^2]
N_{story}	height of the building above grade divided by the height of a single story (-)
NL	Normalized Leakage (-)
NL_{cz}	Normalized Leakage coefficient for each climate zone (-)
size	Floor area divided by the reference area of ($100m^2$) [$1000\ ft^2$]
ϕ	Model coefficient (-) for property indicated by subscript
P	Probability (-) Is zero if it does not have property indicated by subscript; is unity if it does.

Subscripts:

Eff	Designates Energy-Efficient construction
Floor	Floor leakage possibility (e.g. vented crawlspace)
Height	Height of house above grade
LI	Designates Low-income

For equations 3-10:

A_C = leakage area in the ceiling plane [m^2]
A_F = leakage area in the floor plane [m^2]
A_o = total leakage area of the structure [m^2]
C = wind shielding class parameter
Q is the airflow [m^3/s]
A,B = terrain parametes
h= height of structure [m]
T_o = inside temperature [295 K]
g = acceleration of gravity [$9.8m/s^2$]
I_i = air change rate in the i^{th} time step
Δt = length of each discrete time period [s]