AIVC 10913

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Smoke Control Basics

Recorded February 19, 1996

Chair:	James S. Buckley, P.E. Michaud, Cooley, Erickson
Presentation 1:	"Basic Approaches to Smoke Management" John Klote, Ph.D., P.E. NIST
Length:	30:35
Presentation 2:	"Considerations in the Application, Selection, and Specification of Fire Safety Related Dampers" Michael L. Wolf, Ph.D., P.E. Greenheck Fan Corporation
Length:	29:34
Presentation 3:	"Smoke Control Systems Damper Components Requirement" Francis J. McCabe, Ph.D., P.E. Prefco Products, Inc.
Length:	21:44
Presentation 4:	"Smoke Management System Design—Where to Start?" William A. Webb, Ph.D., P.E. Rolf Jensen & Associates, Inc.
Longth	20.25

Length: 30:35

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Fundamentals of Smoke Control

February 1996

John H. Klote National Institute of Standards and Technology Gaithersburg, MD

Acceptance Testing - The Major Smoke Control Problem?

Symptom Not the Problem

Some of the Problems:

Lack of Planning

Overly Complicated System

Unrealistic Expectations

Mechanisms of Smoke Management

Compartmentation

Dilution

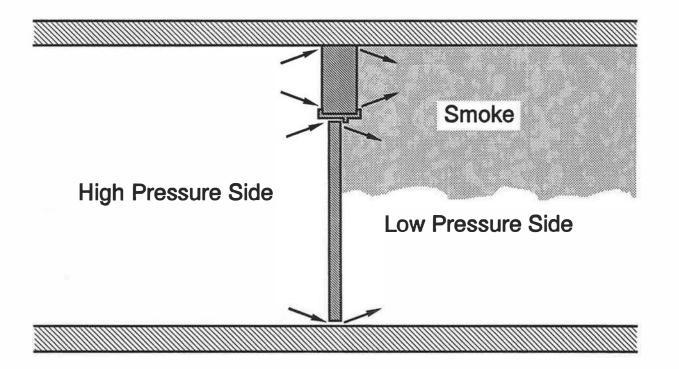
Air Flow

Pressurization

Buoyancy

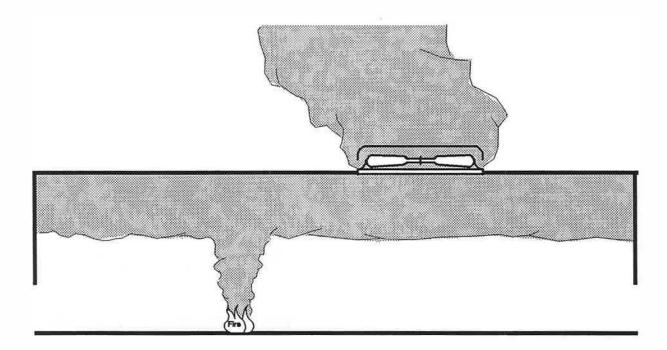
Pressurization

ΔP Across a Barrier ASHRAE Smoke Manual & NFPA 92A



Buoyancy

Malls, Atria, Large Spaces



Some Smoke Control Systems

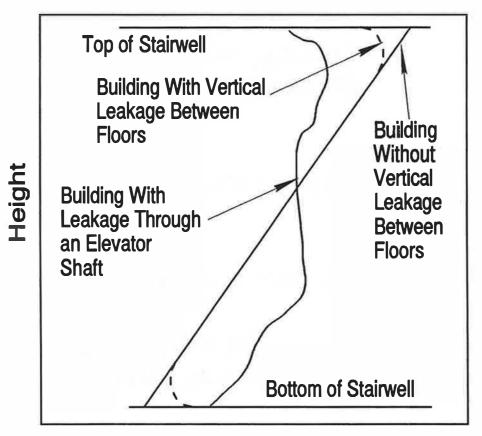
Stairwell Pressurization

Elevator Pressurization

Zoned Smoke Control

Atrium Exhaust (Really Smoke Management)

Stairwell Pressurization



Pressure Difference

Stairwell Pressurization

Pressurization Range:

Min ΔP - Control Smoke Max ΔP - Door Opening

Major Problem: ΔP Fluctuations due to Open Doors

Several System Approaches (ASHRAE Manual)

Computer Analysis ASCOS (ASHRAE Manual) CONTAM (George Walton)

Elevator Smoke Control

NIST/NRCC Joint Project:

Smoke Control for Fire Evacuation of the Disabled (U.S. Part Funded by V A)

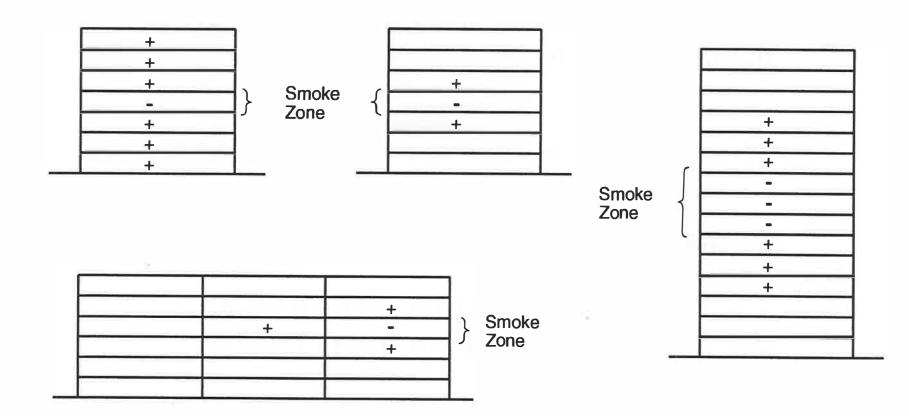
Conceptual Studies of Elevator Smoke Control Systems

Full-Scale Fire Experiments at NRCC's 10 Story Fire Research Tower

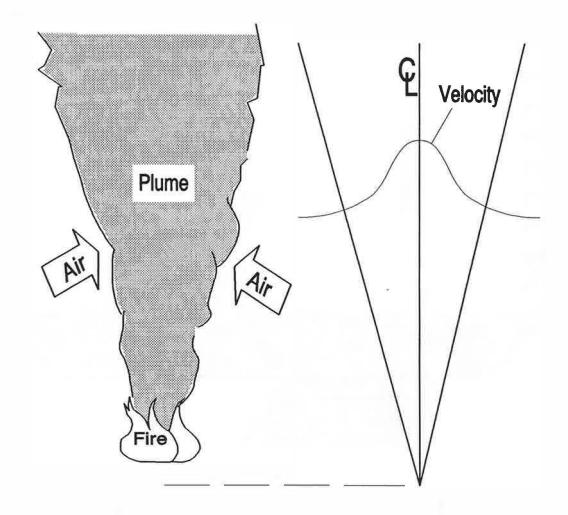
Analysis and Experiments of Elevator Piston Effect

Design Information: ASHRAE Manual

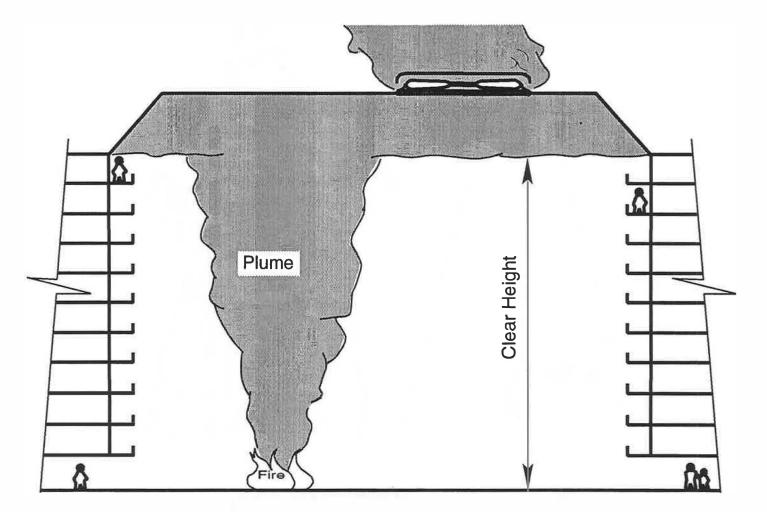
Zoned Smoke Control



Atrium Smoke Control



Atrium Smoke Control



Summary

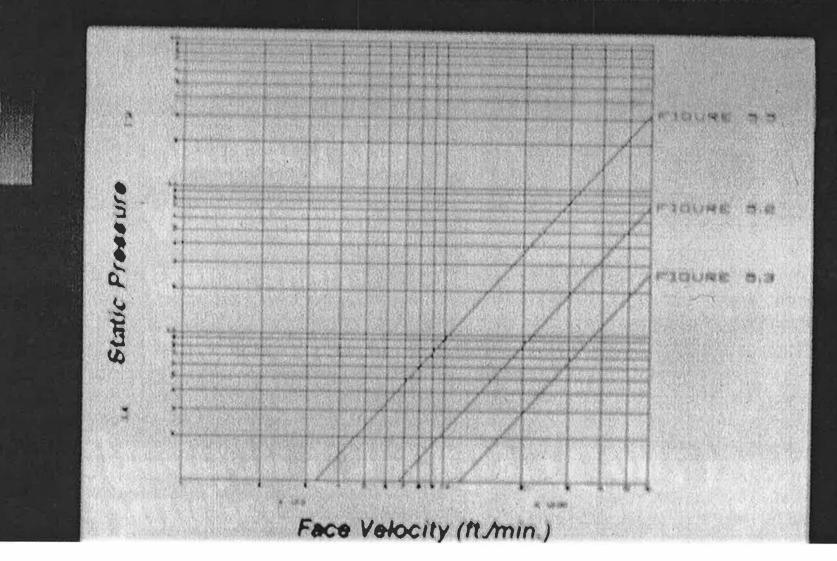
Mechanisms of Smoke Management Compartmentation Dilution Air Flow Pressurization Buoyancy

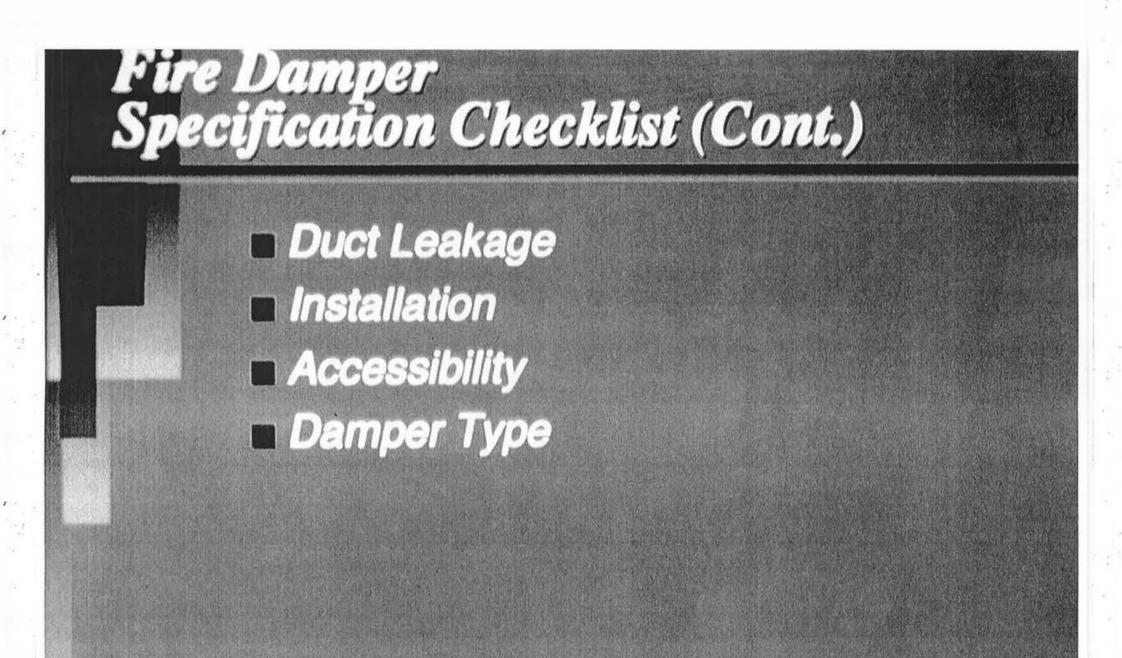
Smoke Control Systems Stairwell Pressurization Elevator Pressurization Zoned Smoke Control Atrium Exhaust (Really Smoke Management)



Each smoke damper shall be equipped with an actuator having an operational airflow rating of at least 110% of the maximum design airflow at its installed location. The operational pressure rating for each damper shall be a minimum of 8 in. w.g. Operational airflow ratings shall be for airflow in both directions through the damper.

Pressure Drop Graph





Smoke Damper Specification Checklist

- NFPA 92A&B/UL555S Classified
- Leakage Classification
- Elevated Temperature Rating
- Operational Airflow Rating
- Pressure Loss
- Installation
- Accessibility
- 🗖 Duct Leakage
- Actuator

Leakage Classification

Smoke dampers shall be UL labeled with a Class I leakage rating. (maximum leakage of 4 cfm per sq. ft. @ 1 in. w.g. and 8 cfm per sq. ft. @ 4 in. w.g.)

OR

Smoke dampers shall be UL labeled with a Class II leakage rating (maximum leakage of 10 cfm per sq. ft. @ 1 in. w.g. and 20 cfm per sq. ft. @ 4 in. w.g.) OR

Smoke dampers shall be UL labeled with a Class III leakage rating (maximum leakage of 40 cfm per sq. ft. @ 1 in. w.g. and 80 cfm per sq. ft. @ 4 in. w.g.)

Elevated Temperature Rating

Smoke Dampers dampers shall be UL labeled with a Temperature Degradation/Cycling rating of (usually 250 °F, 350 °F or 450 °F).

Closure Temperature

Each fire damper shall be equipped with a heat responsive device (e.g. fusible link) which has been tested and approved for use with the damper assembly in accordance with UL Standard 555. The heat responsive device shall have a temperature rating of (usually 165°F or 212°F)



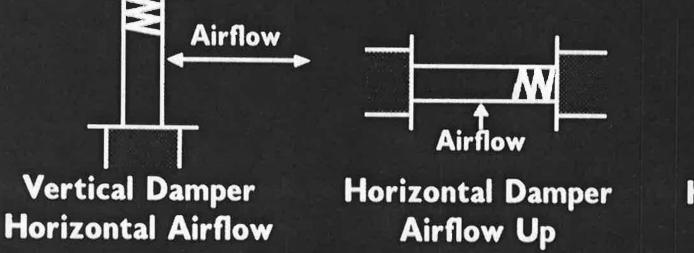
Fire dampers shall be UL labeled for use in static systems.

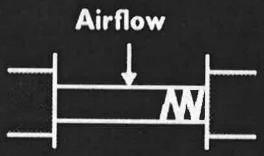


Fire dampers shall be UL labeled for use in dynamic systems.

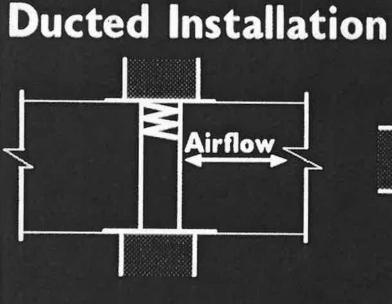
System Rating (Cont.)

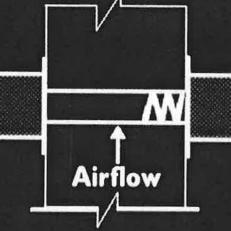
The dynamic closure rating for each damper shall be at least 110% of the maximum design airflow at its installed location. The dynamic closure pressure rating for each damper shall be a minimum of 8 in. w.g. Ratings shall be for airflow in either direction through the damper.

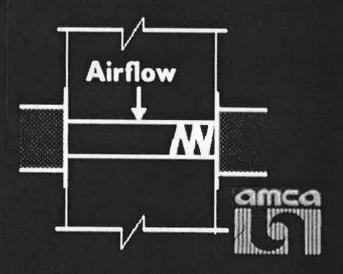




Horizontal Damper Airflow Down

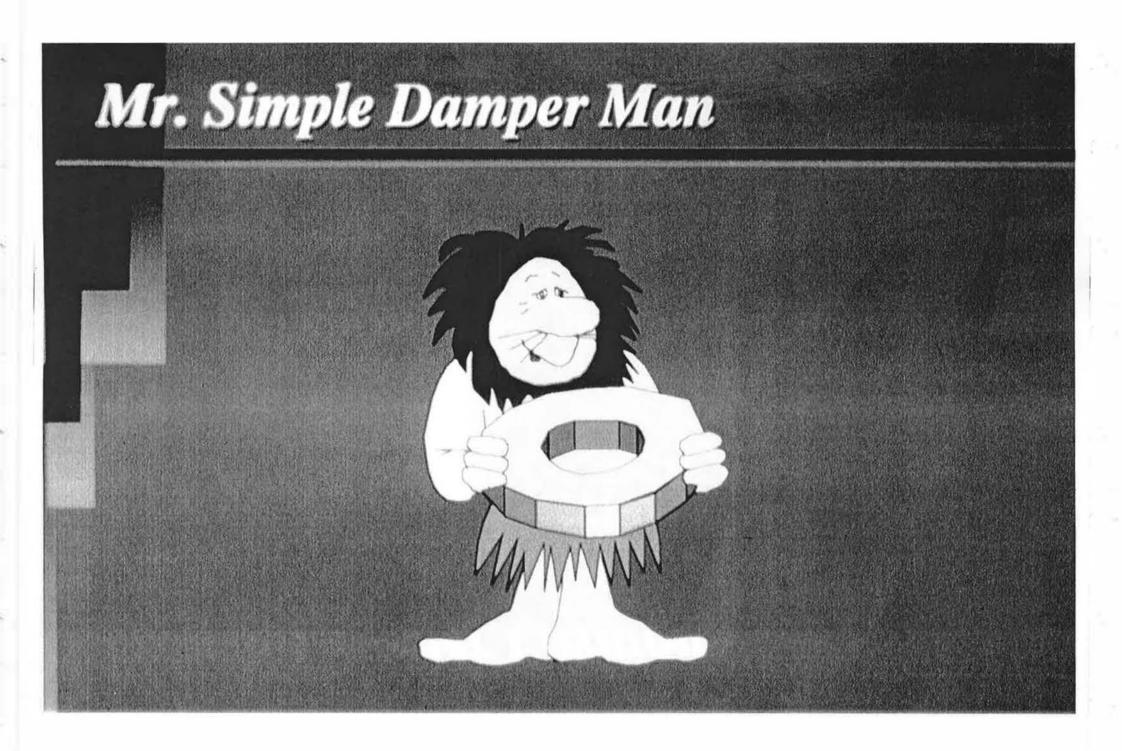


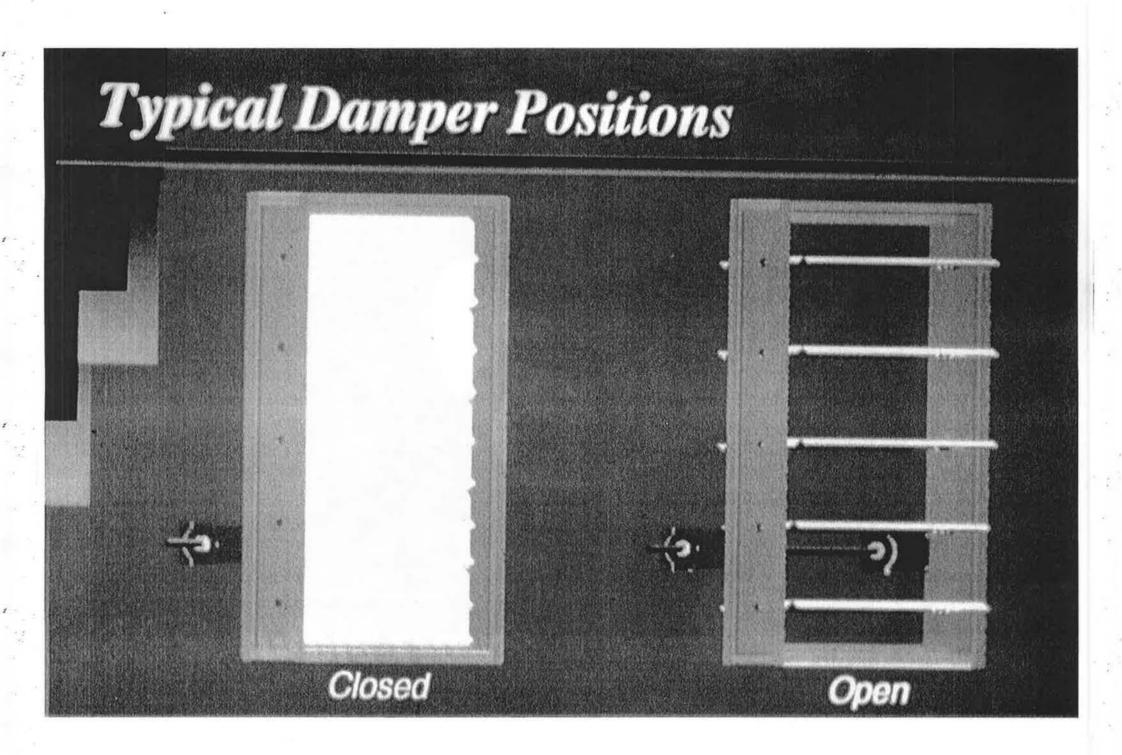




Pressure Loss

Manufacturer's submittal information shall include a graphical representation of duct velocity vs. pressure drop across the damper. The graphical representation shall include data for a 12x12 damper, 24x24 damper, and 36x36 damper tested in accordance with the latest edition of AMCA Standard 500 and shall include data for test figures, 5.2, 5.3, and 5.5.





Fire Damper Specification Checklist

NFPA 90A/UL555 Classified Hourly Fire Rating System Rating Closure Temperature Pressure Loss Duct Leakage Installation Accessibility Damper Type

NFPA 90A/UL555 Classified

All fire dampers shall meet the requirements of NFPA 90A and shall be tested, rated and labeled in accordance with the latest edition of UL Standard 555. The contractor shall submit the manufacturer's data sheets and installation instructions detailing compliance with these specifications.

Hourly Fire Rating

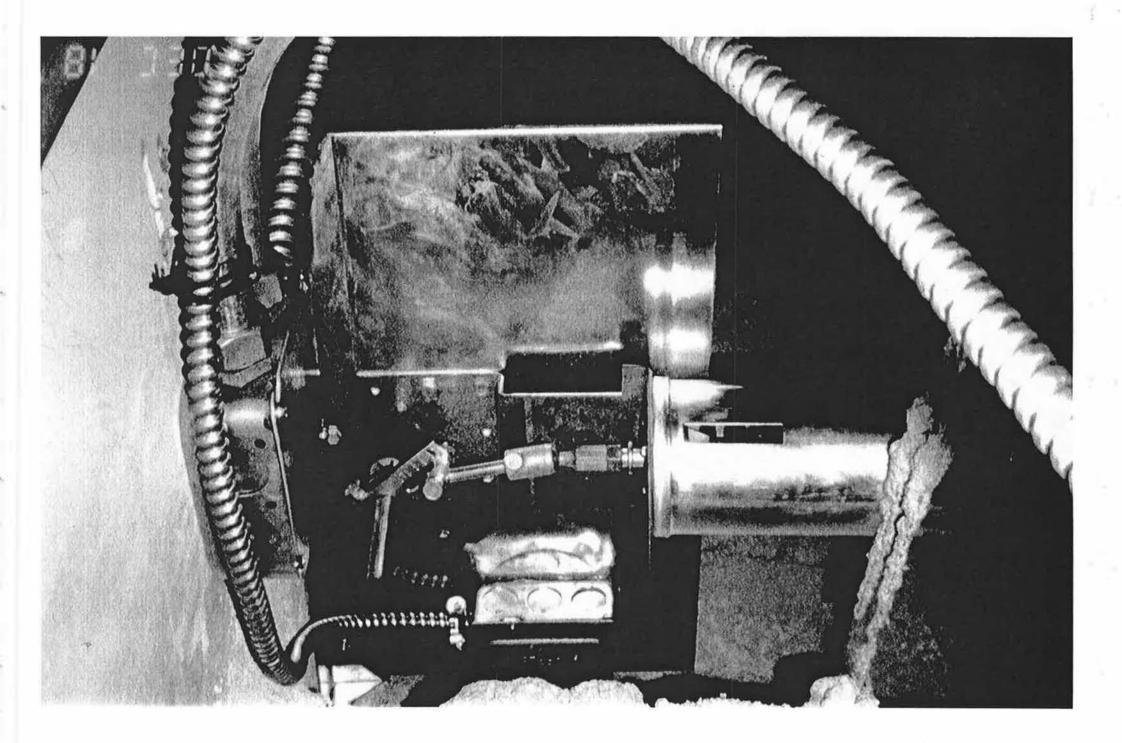
Fire dampers shall be UL labeled with a 1-1/2 hour fire rating.

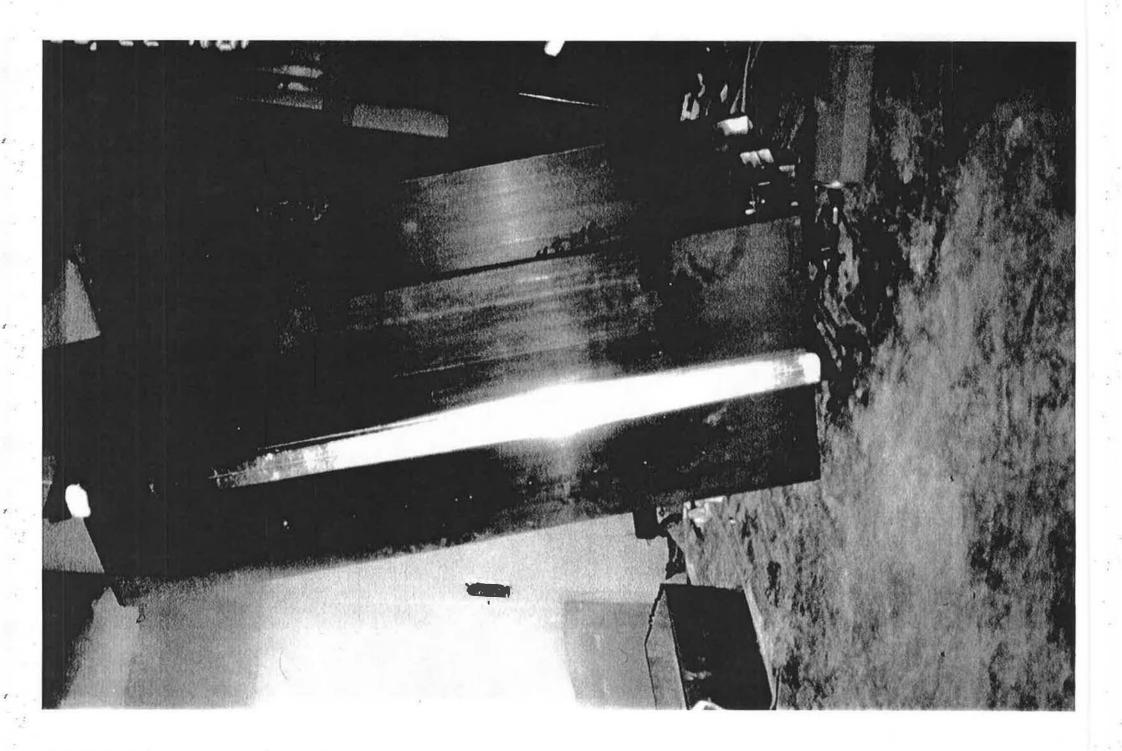


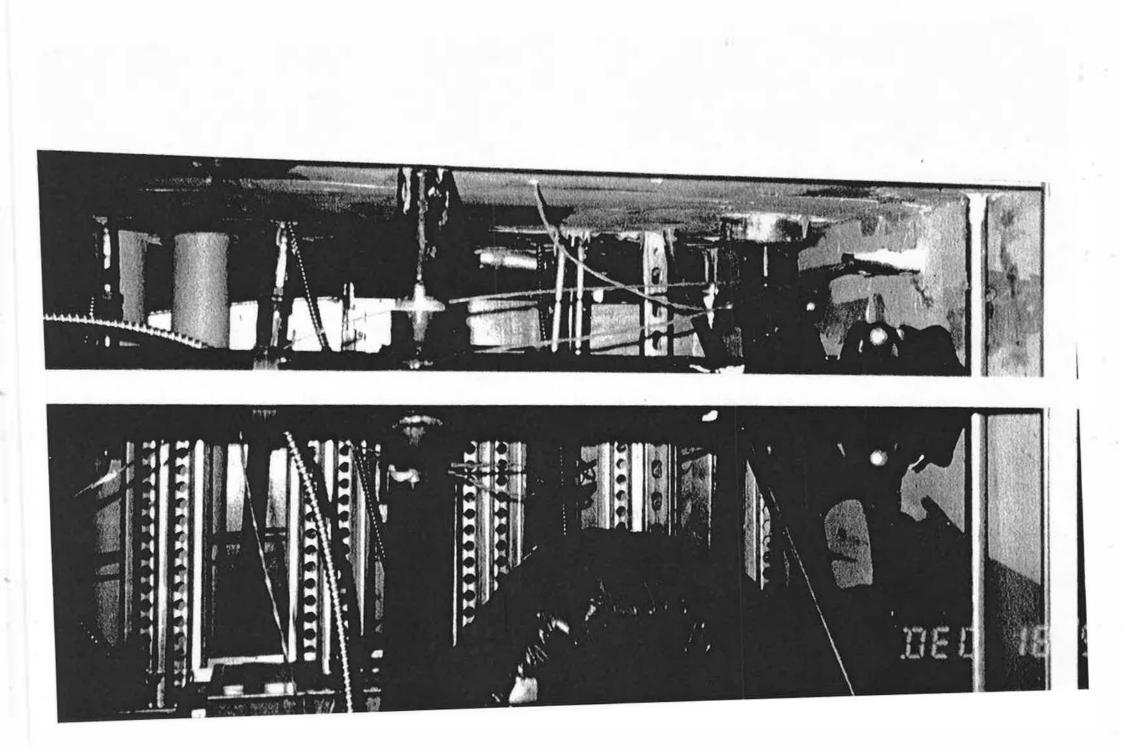
Fire dampers shall be UL labeled with a 3 hour fire rating.

Actuators

Actuators shall be factory installed. Manufacturer's submittal data shall indicate actuator space requirements around the damper.



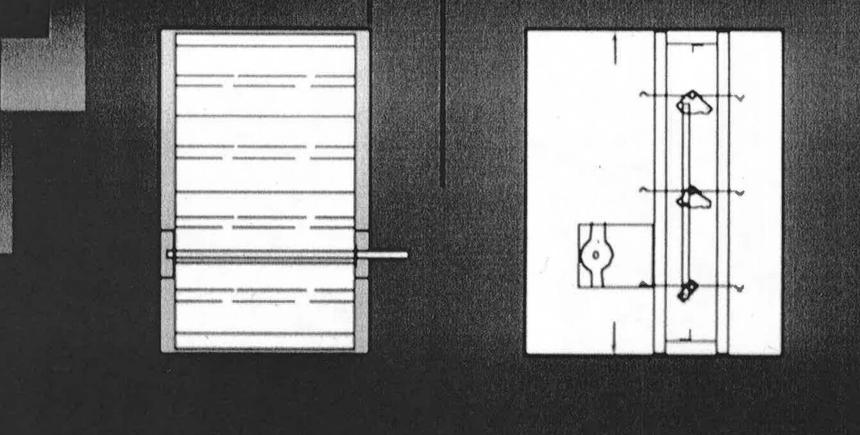


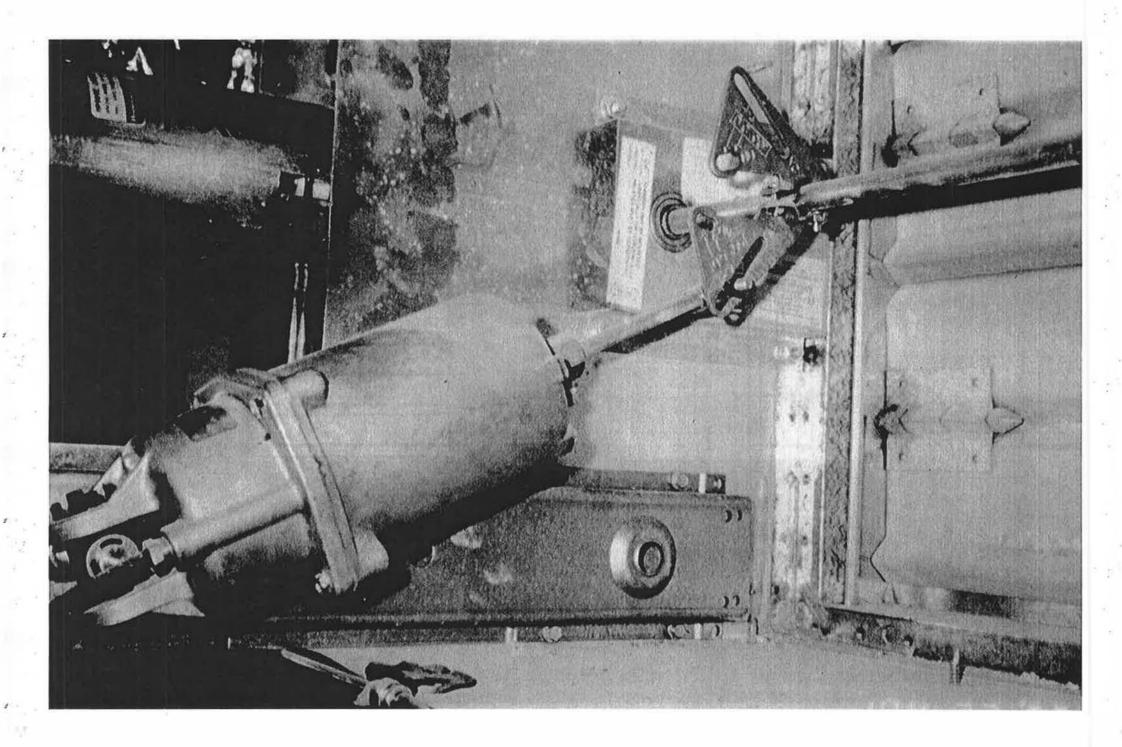


Fire Damper Specification Checklist Smoke Damper Specification Checklist Installation Guidelines

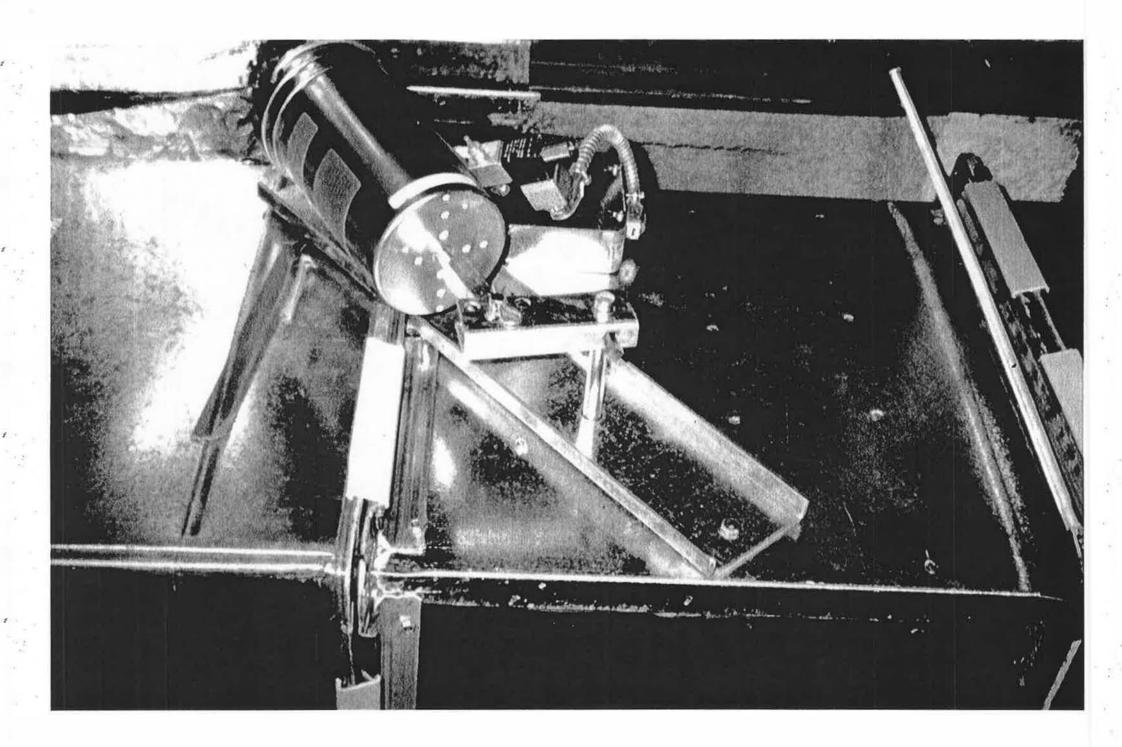
Damper Application Issues



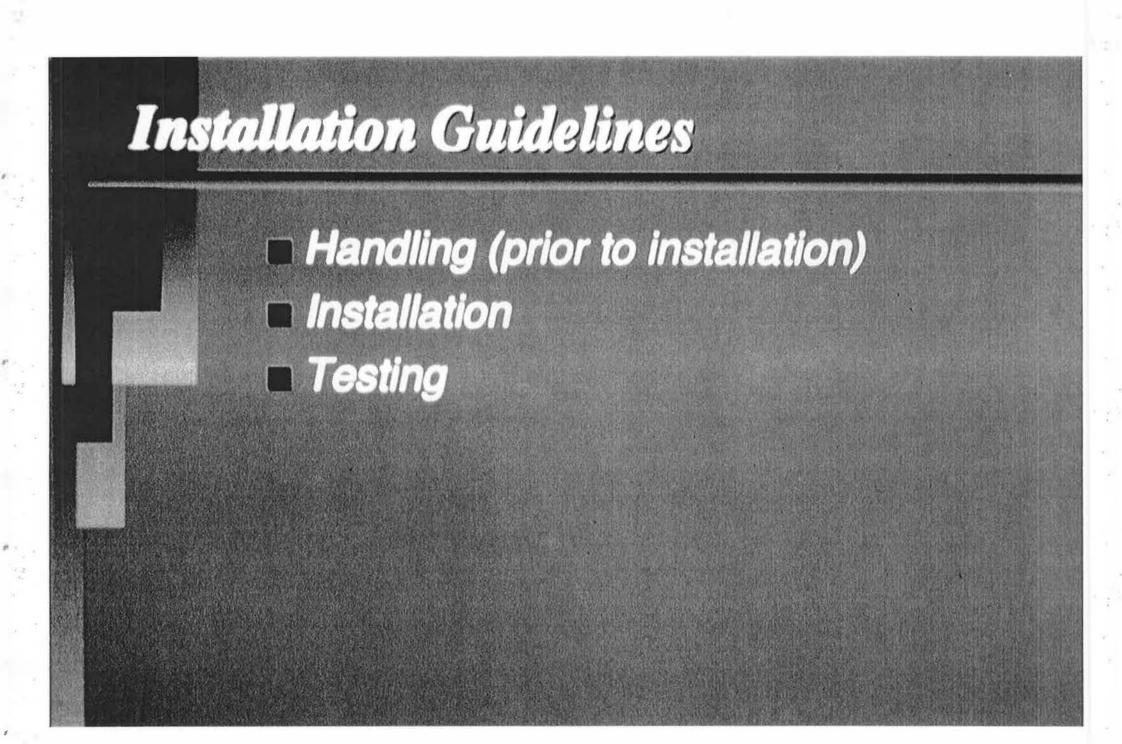












Smoke Control Systems Damper Components (1)

- 1. PRESSURIZATION In order of pressure gradients (from negative fire zone):
 - a. Occupied zones (lowest positive (+) pressure)
 - b. "Sandwich" areas around fire zone (+),
 - c. Escape routes (corridors (++), vestibules (+++), stairwells (++++) -- higher as you go out),
 - c. "Sandwich" areas around fire zones (+), and
 - d. Refuge areas, disabled persons safety spaces; fire fighters control and staging areas... etc..(++++)

Smoke Control Systems Damper Components (2)

2. Low temperature PURGING - while components such as dampers, fans, and detectors still work (at least up to 450°F); in zones that received smoke input in the incipeint stages of the fire prior to the establishment of pressurization differentials -- or as a stand alone mode; e.g., for atria smoke control +.

Smoke Control Systems Damper Components (3)

3. EXHAUST - De-pressurizing the fire zone is as critical as lowering fire temperatures in guaranteeing the success of the "pressure sandwich" and escape route pressurization systems. Some smoke may also be removed. (See ASHRAE Paper No. 3427 (RP559).

In transitioning from 'active' smoke control modes the return or exhaust damper(s) must never close without causing or having the fire room supply dampers closure also -- smoke spread would result.

Smoke Control Systems Damper Components (4)

4. CONTAINMENT - The last stand where the smoke control system damper components that are in the fire barriers around the fire zones are closed to maintain barrier ('passive') integrity, just before their operating ratings (temperature limits) are reached.

This is also a critical fire control (barrier) mode. ('Passive') positive fire pressure is contained by the now passive (no mechanical) fire energy.

Smoke Control Systems Damper Components (5)

5. Smoke PURGING after the fire on a components survivability basis. This is a very slow smoke clearing operation that would have little relativity to pressure dynamics -dampers would be full open and fans to 100%.

Smoke Control Systems Damper Components (6)

N.B. No fire room return or exhaust damper should close (on elevated temperature) without signaling closure of the fire room supply damper -- or smoke would be spread by positive pressure in the fire room, the initial fire damper operation concept is a critically wrong action as the return/exhaust damper is certianly going to close first if it is fitted with a fire damper heat responsive device.

Smoke Control Systems Damper Components (8)

GENERAL DAMPER OPERATING TEMPERATURES PER SYSTEMS MODES (& STATUS)

Ambient (active)	Pressurization& Purge
Low Temp.	Exhaust &
(Ambient - 450°F)(active)	Pressurization
Medium Temp.	(Passive) Smoke
(450°F - 850°F)	(& Fire) Containment
High Temp.	Fire Containment
(850°F - 2000°F)	(& Smoke Per ISO)

The damper designer/Manufacturers goal would be that one combination air/smoke/fire damper design would handle all the above performance parameters in all of the systems modes of operation.

Smoke Control Systems Damper Components (7)

- General Damper Design Criteria as to Smoke Systems Requirements:
 - A) Ambient 450°F 'active' smoke system modes operation/actuation (fans, & etc., on) cycling capability.
 - B) 450°F 850°F 'passive' smoke & fire containment.
 - C) To 2000°F fire barrier (tighter seals to meet ISO (Internaltional) Standards).
 - D) 8" W.G. (ambient) systems supply pressures & 4" systems return pressures cycling & leakage tests.
 - E) (Pressurization) leakage rates (ambient) of 170 CFM/FT² supplies, and 120 CFM/FT² returns --Class IV.
 - F) 32" W.G. transient pressure closure (rapid) possiblity -- or 'spike' precluded by 3 second minimum closure.
 - G) 2000-5000 FPM system ambient flows.
 - H) 3000-7000 FPM heat expanded flows.
 - .5" W.G. sprinklered & unsprinklered fire room ('passive') pressure.
 - J) 28 CFM/FT², Class III 'passive' leakage.
 - K) 1/16"/FT at full fire heated blade expansion while maintaining leakage rated performances to 'active' and passive requirements.
 - L) 15 second closure and 90 second opening cycle time.
 - M) 25 LB.IN./FT² operating torque.
 - N) G90 corrosion resistance (or other specific atmosphere) exposure & cycling.

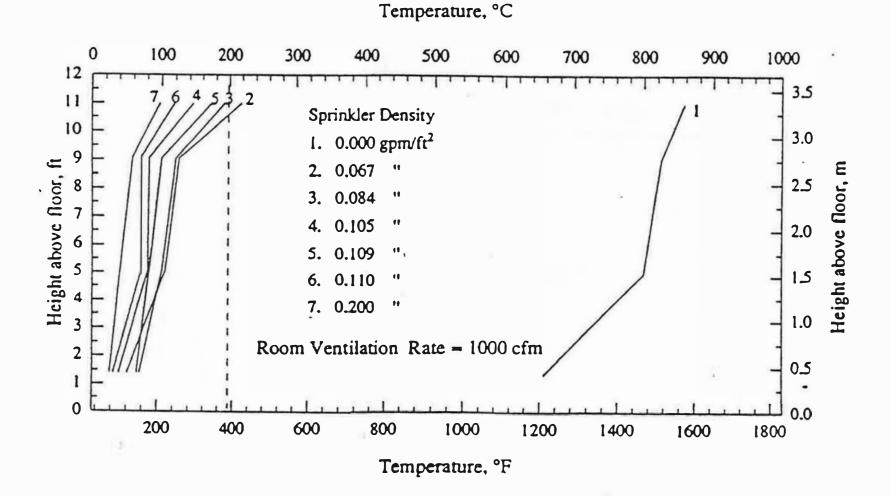


Figure 6 Temperature profiles at north thermocouple tree in the one-story test room for different spray application rates, for ventilation rate of 1,000 cfm (0.42 m^3/s).

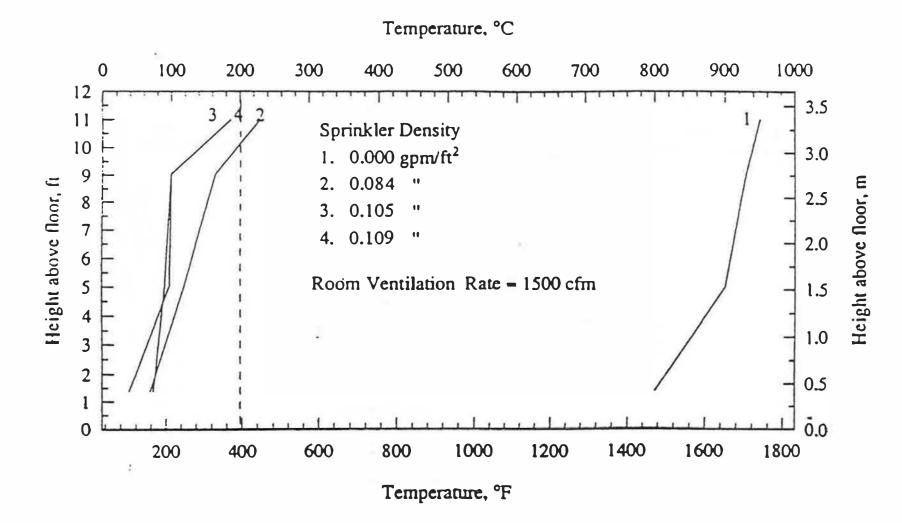


Figure 7 Temperature profiles at north thermocouple tree in the one-story test room for different spray application rates, for ventilation rate of 1,500 cfm (0.63 m^3/s).

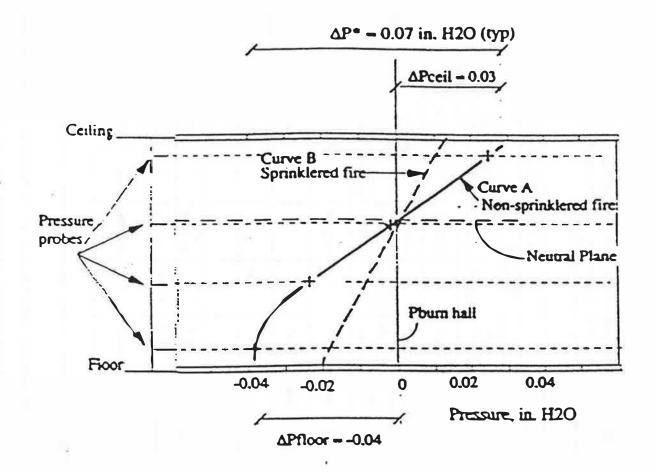


Figure 8 Typical pressure profiles in the one-story test room for a sprinklered and a nonsprinklered fire.

TABLE 1

SMOKE SYSTEMS FUNCTIONS WITH DAMPER POSITIONS AND REQUIRMENTS

VIS-A-VIS Amb. - 450° Active, 450° - 850° Passive (to 2000° Fire under ISO) (Needs full development by ASHRAE TG5.SMC)

SMOKE SYSTEMS FUNCTIONS / SITUATION (See Figure 1)			DAMPER POSITION		DAMPER PERFORMANCE REQUIREMENTS											
			DAMIT ETT TO STITION			SUPPLY			EXHAUST Note (1)							
FUNCTION	ZONE	PHASE	CONTROL	ZONE TEMP- ERATURE	SUPPLY	DEDICATED VENT NOTE (2)	EXHAUST	TEMP- ERATURE	SYSTEM PRESSURE	VELOCITY/ LEAKAGE AT DAMPER	L EAKA GE PRESSURE	TEMP- ERATURE	SYSTEM PRESSURE	VELOCITY/ LEAKAGE Note (3)	LEAKAGE PRESSURE Note (4)	TRANSIENT PRESSURE 32" Pos.
PRESSURIZATION (FULL BUILDING)	"A" (Non-Fire No Smoke)	-	Automatic	Ambient	Open	Closed	Closed	Ambient	8"	2-5000FPM	N/A	Ambient	-3*	2/ 120CFM/FT ²	4ª	DA
PRESSURIZATION (SANDWICH ONLY)	"A" (Non-Fire No Smoke)	Adj. to C1 & C2	Automatic with Fire Fighter Supervision	Ambient to 450°F	Open	Closed	Closed	Ambient	8'	2-5000FPM	N/A	450°F	-2'	3/ 120CFM/FT ²	4	T A
	A" (Non-Fire	-	Autometic	Ambient	Open with pressure set	Controlled to set pressure	Closed	PRE	SURE SET	OPTIONAL		PRE	SSURE REI	EASE OP	IONAL	. D E
	No Smoke)							Ambient	0.8ª	1-5000FPM	Sel .04-0.45	Ambient	Set .04-0.45	Set .0445'	NA	
PURGE (AIR CHANGES)	*B* (Non-Fire With Smoke)	-	Fire Fighter Control - Maintain Positive Pressure	Ambient to 450°F	Open	Open	Open	Ambient	8'	2-5000FPM	N/A	450'F	-3" ·	3-7000FPM	N/A	EL
EXHAUST	"A" (Non-Fire No Smoke)	C1	Automatic with Fire Fighter Supervision	Ambient to 450°F	Closed Nole (2)	Open	Open	Ambient	-3'		4	450°F	-2"	3-7000FPM	N/A	P M E
PURGE (AIR CHANGES) NOTE (3)	"C"Fire Zone	C1	Before 450°F (Automatic and/or with Fire Fighter Supervision-Maintein Negative Pressure	Ambient to 450°F	Open	Open	Open	Ambient	8"	2-5000FPM	N/A	450°F	-2	3-7000FPM	N/A	N T O
CONTAINMENT NOTES (5) & (6)	C'Fire Zone	C2	Automatic	450°F to 2000°F	Closed	Closed (or Open By Fire or Supervision)	Closed	450'F	8.	170/ 29CFM/FT ²	8"	450°F	-2	3/ 120CFM/FT ²	4*	G
								2000°F	0.2" or .03"	/ 12CFM/FT ²	.5'	850°F (or 2000°F ISO)		1/ 200CFM/FT ²	.5*	0
PURGE (RE-0PEN FOR AIR CHANGES) NOTE (7)	'C'Fire Zone	Сз	Under 150°F (Fire Fighter Supervision Recommended	Below 150°F	Open	Open	Open	Ambient	8'	2-5000FPM	NA	Ambient	-3'	2-5000FPM	N/A	G Note (8)

NOTES:

(1) Some codes require that supply air continues to flow into the fire zone, for cooling, during the exhaust mode (Max. 50% of exhaust ambient volume capabilities essential to maintain negative pressure in the fire zone).

(2) Venting is a design alternate covered by NFPA 92A & 204M.

(3) The test leakage rates based on ambient Class III 1" @ 40CFM/FT^a as converted from (elevated) temperature & .5 pressure requirements and Class IV (or greater for ambient pressurization) 8" & 4" supply and return requirements).

(4) The main leakage requirement is when pressurization is lost and the damper must act as part of the physical bearrier system around the fire zone for contaiment. This function could be called 'passive' (leakage) smoke control; and leakage tested to 450°F (min), (0.2° W.G. unsprinklered and .03 sprinklered fire room conditions) @ 0.5° W.G.

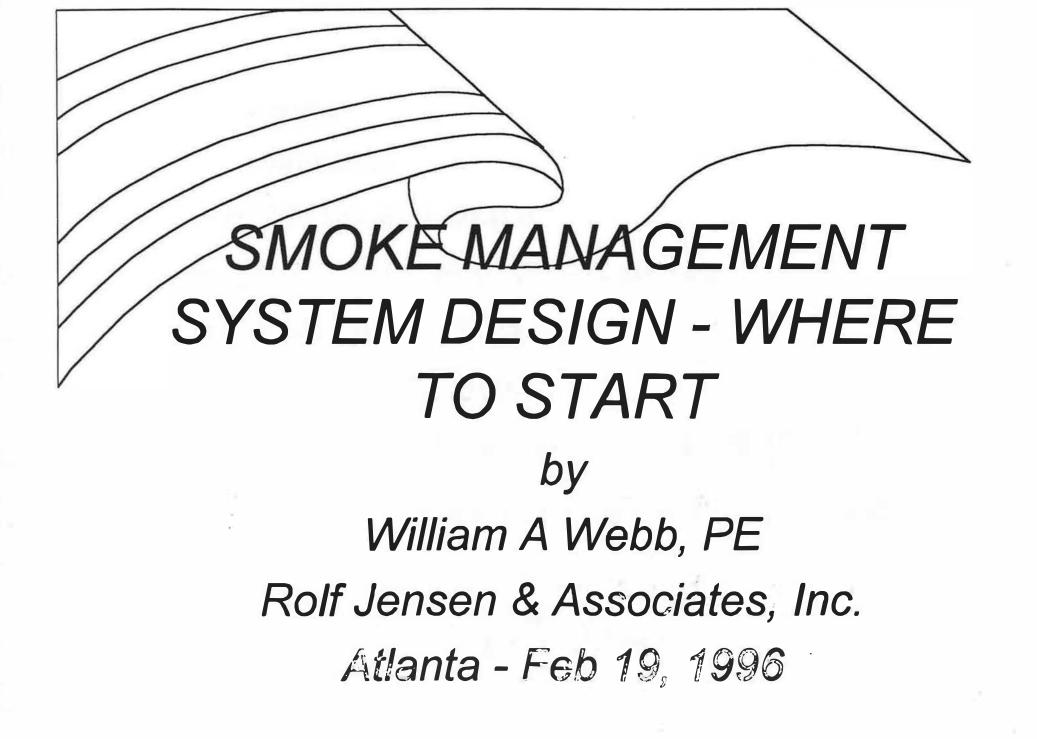
(5) It is probable that, with most sprinklers & fire fighter suppression the only damper position change will be automatic closure for containment from the initial fire and smoke locations damper settings.

(6) Closure for containment must have synchronous closure of supply with return damper while pressurization is 'active' to avoid accidental smoke spread.

(7) This re-open function is on an assumed component survivability basis.

(8) Translent pressures may be eliminated as a problem by requiring a minimum closure time of 3 seconds.

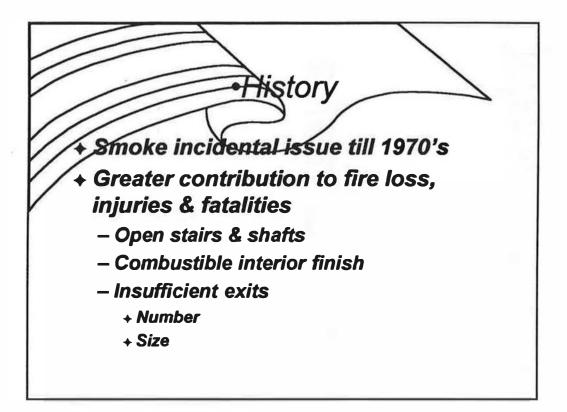
(9) Damper operating times need development as to system modes need with economics considered.



 Smoke incidental issue till 1970's
 Greater contribution to fire loss, injuries & fatalities

History

- Open stairs & shafts
- Combustible interior finish
- Insufficient exits
 - + Number
 - + Size



ん

Development of codes

Save the city-prevent conflagration

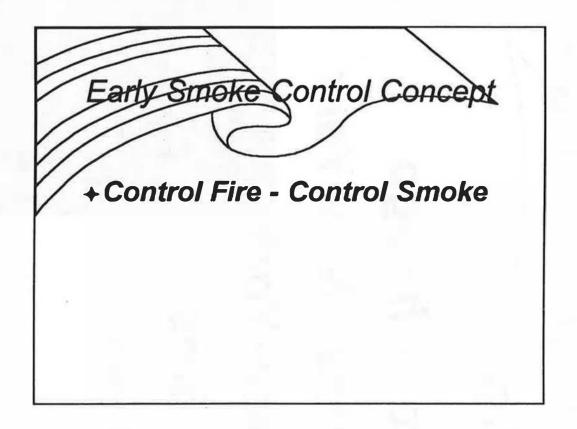
Save the building

Save the floor

Save the life

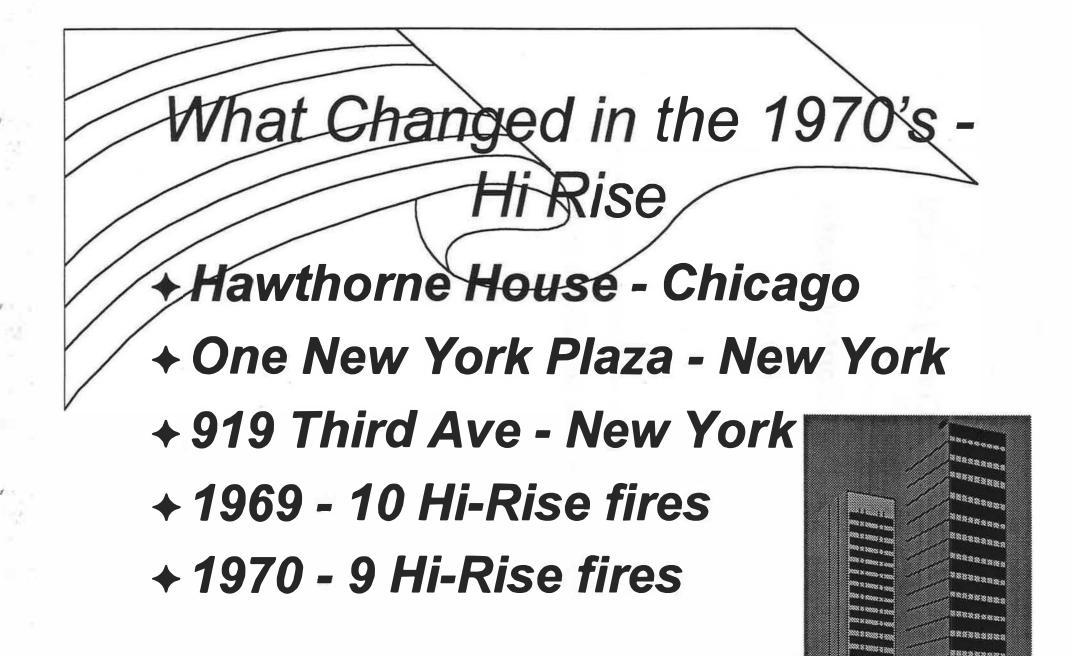
Smoke not an issue till set goal to save the floor



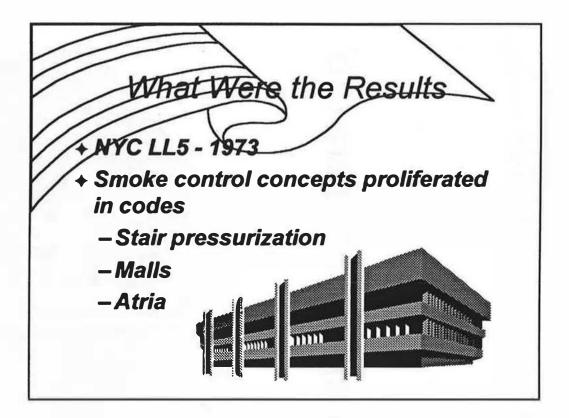


Many still advocate this as the most effective strategy

3



********** ********** ***********



LL5 had many features in addition to smoke control. Sprinklers or compartmentation

<u>New</u> <u>Existing</u> Smokeshaft Smokeshaft

or

Pressurized stair

No smokeshaft, pressurized stair or compartmentation w/AS

+ NYC LL5 - 1973 + Smoke control concepts proliferated in codes

Were the Results

- Stair pressurization
- -Malls
- Atria

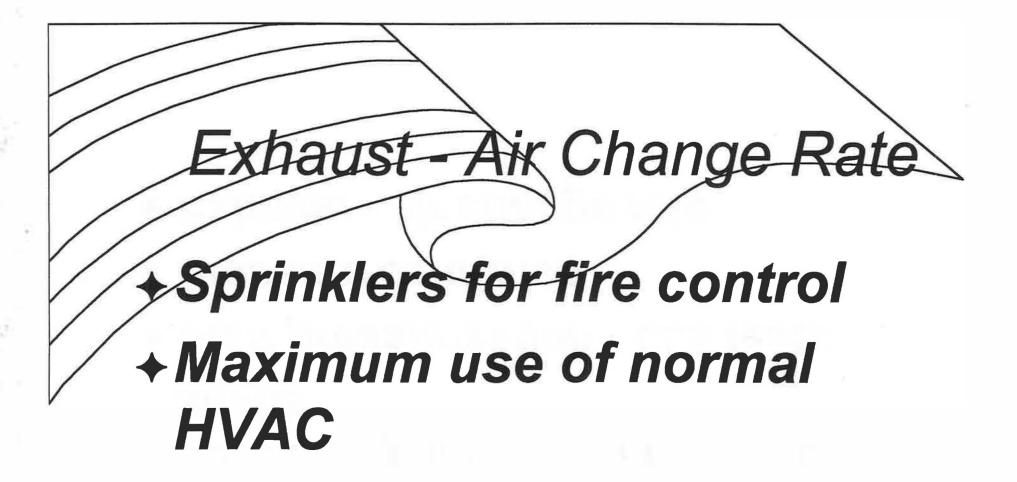
Shutdown HVAC Vent thru panels or windows or shafts

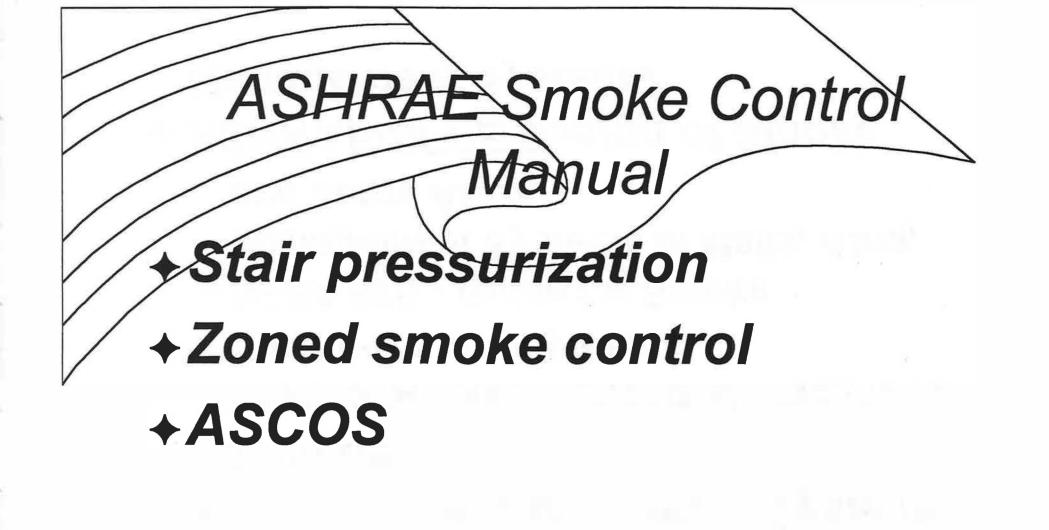
+ Stair pressurization - LL5 tests

Smoke Control

Concepts

- + Pressure sandwich
- + Exhaust air change rate





Recent Developments

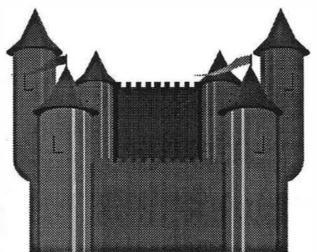
NFPA Smoke Management Systems Committee

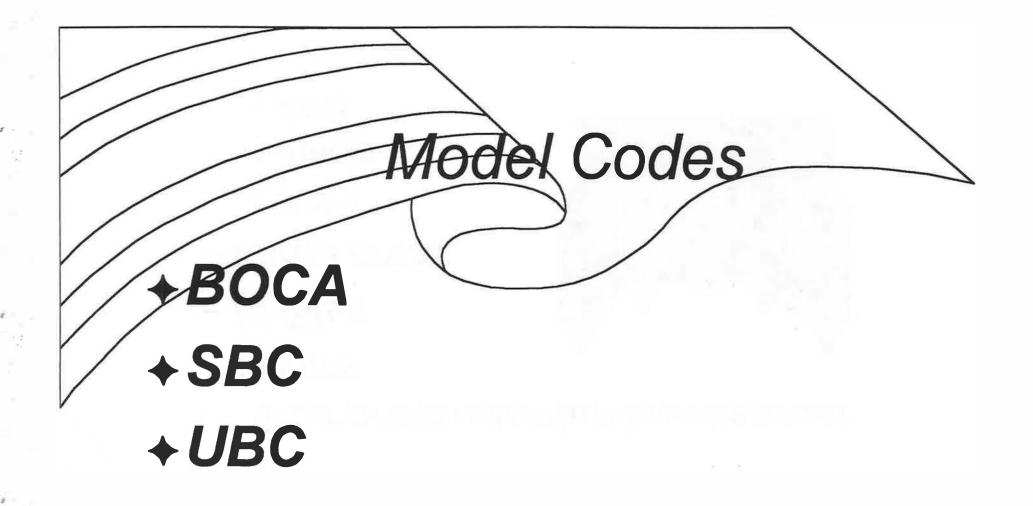
- NFPA 92A Recommended Practice for Smoke-Control Systems
- NFPA 92B Guide for Smoke management Systems in Malls, Atria, and Large Areas
- + ASHRAE/SFPE Design of Smoke Management Systems

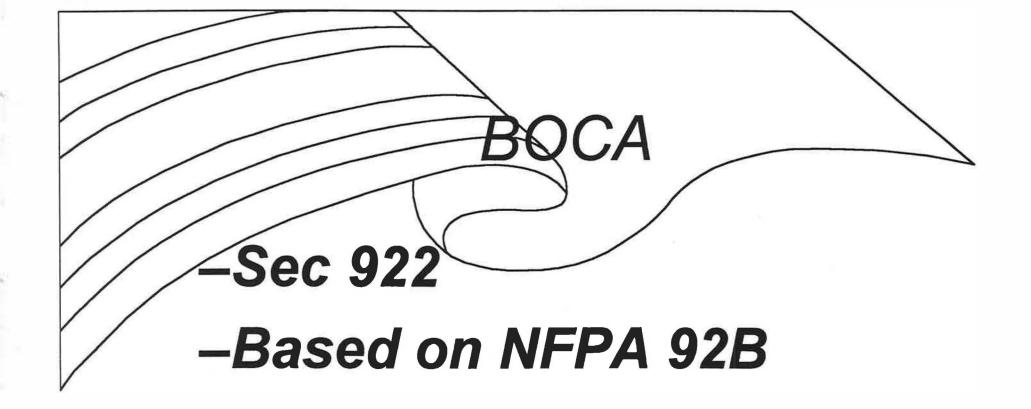
Smoke management in 3 general areas

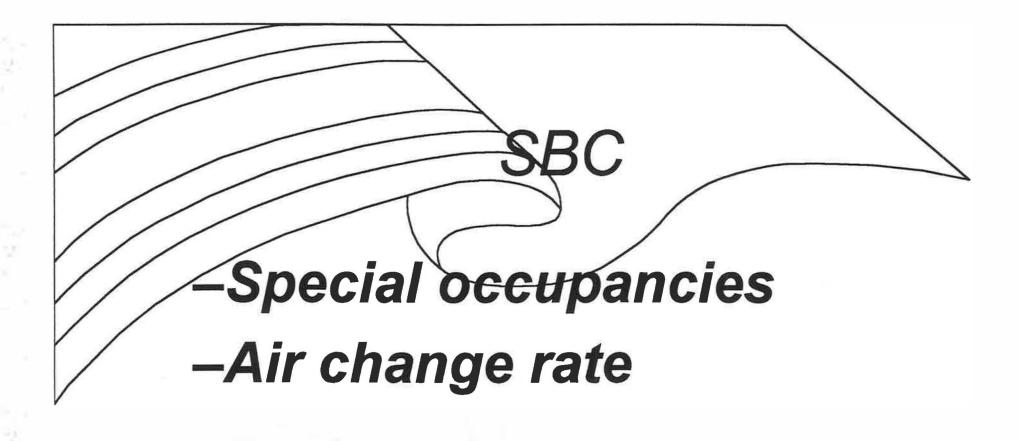
Sodes

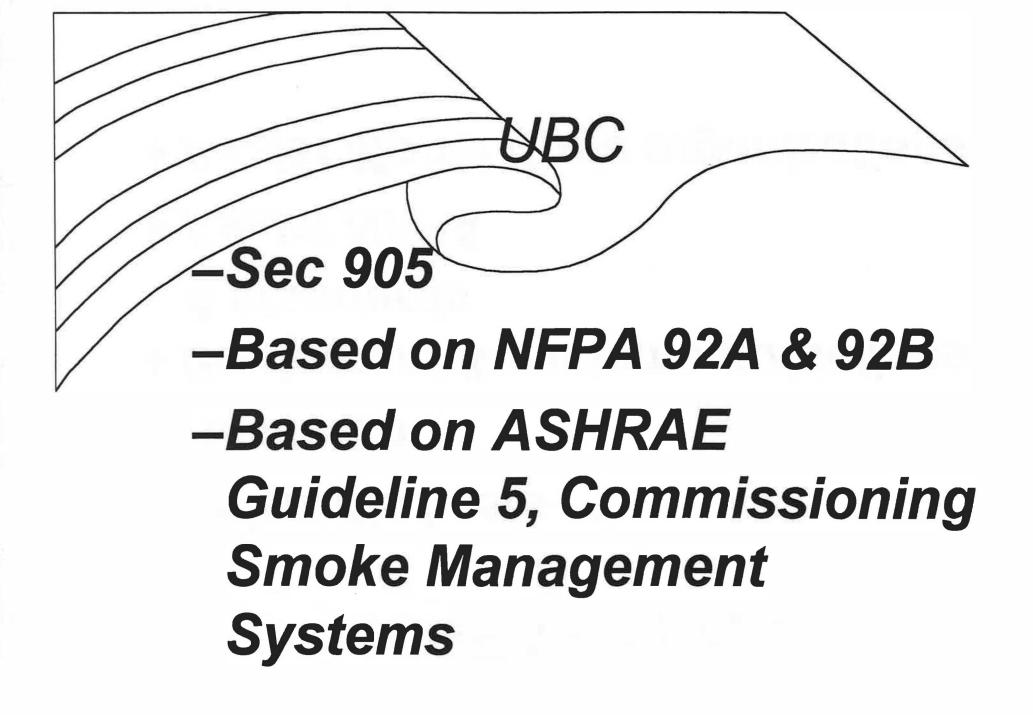
- Stair pressurization/smokeproof towers
- Hi-Rise
- Large areas
 + Malls
 + Stadia
 + Atria











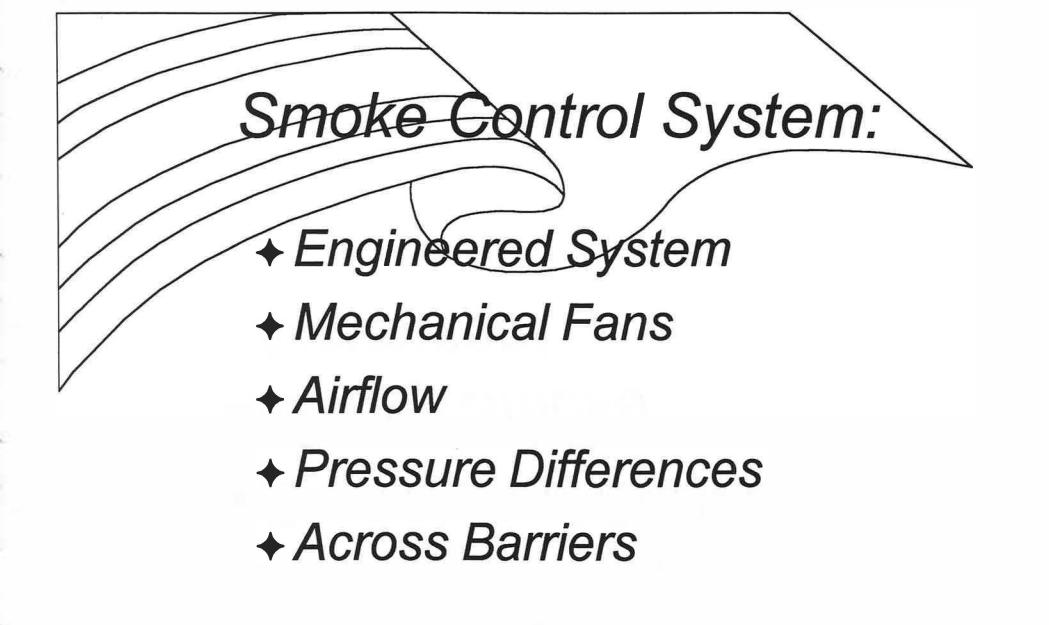
Scientific basis
 Research

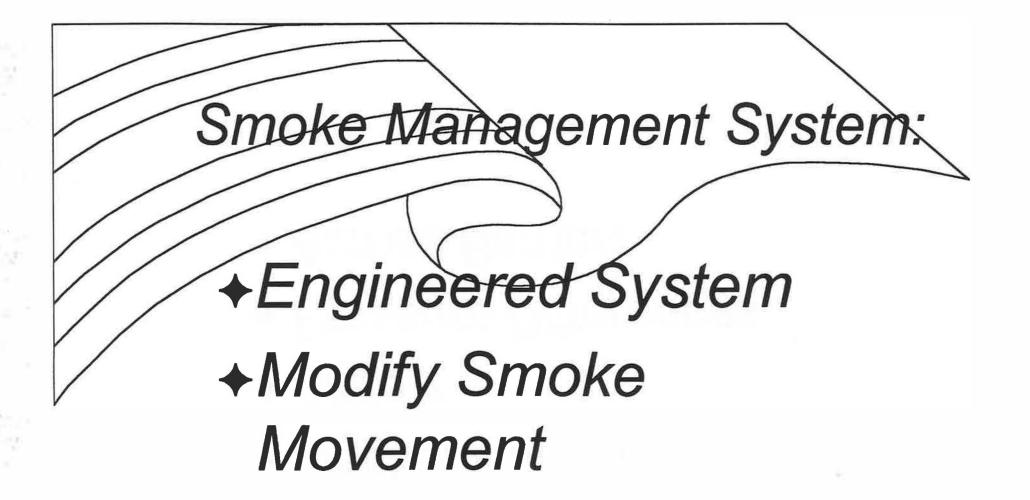
Equipment & systems guidelines
 & standards

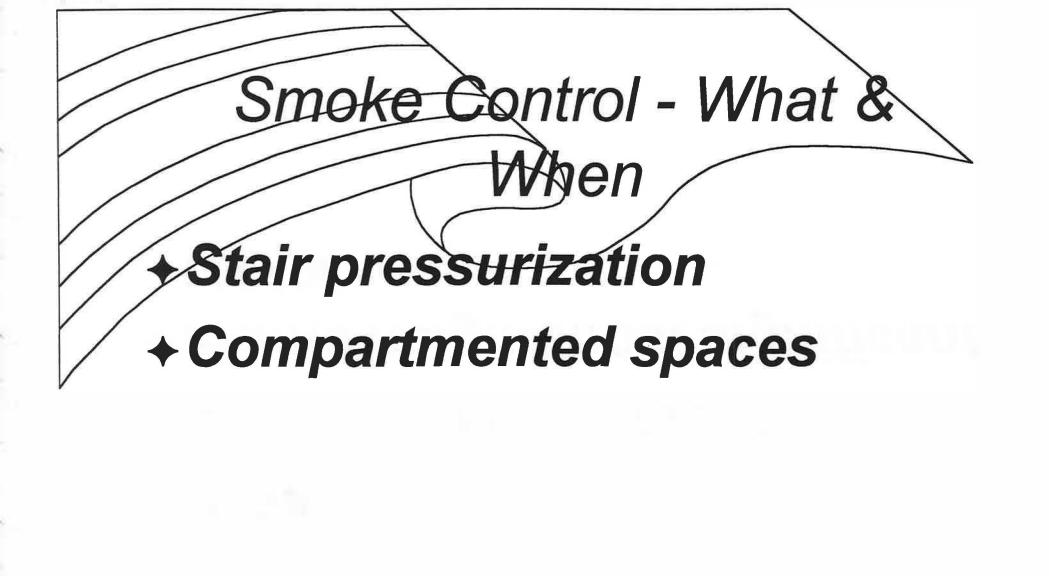
Re's Role

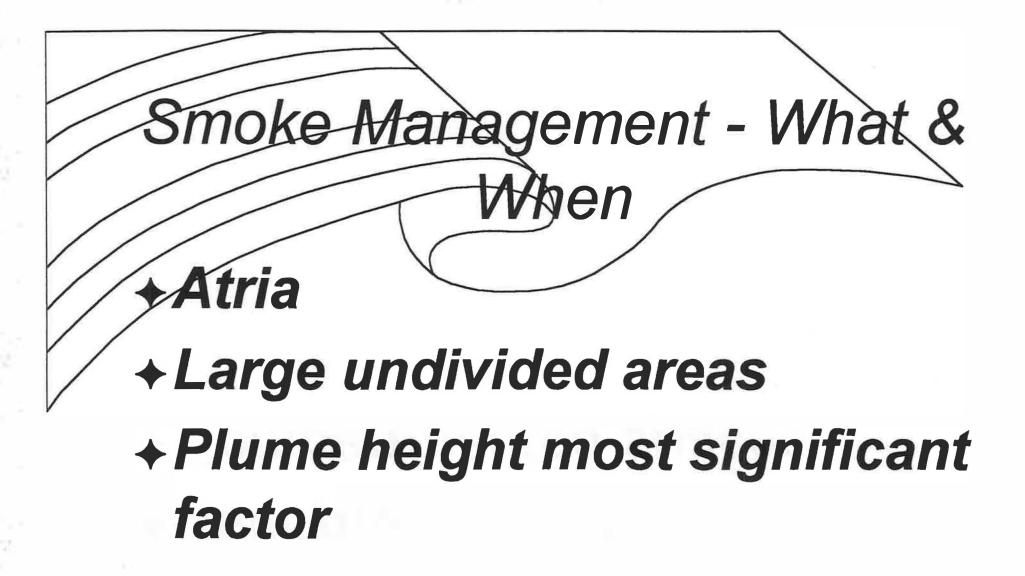
+ Assist NFPA

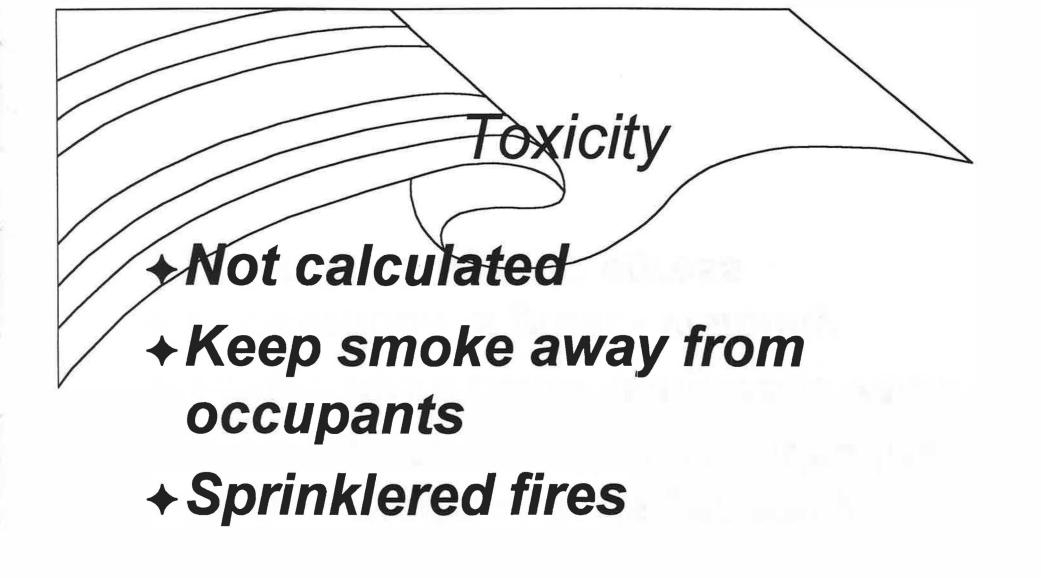
+ Assist Model Code organizations



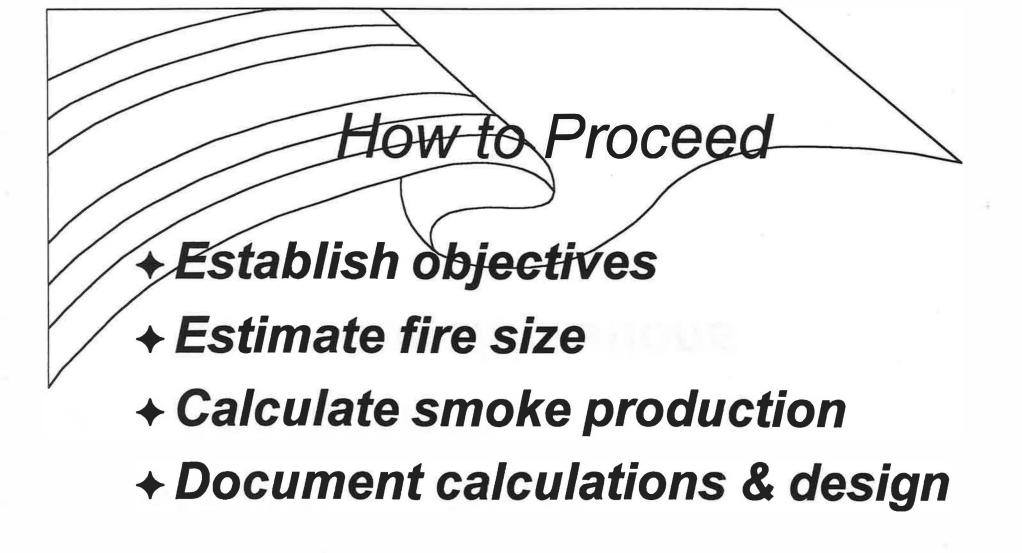


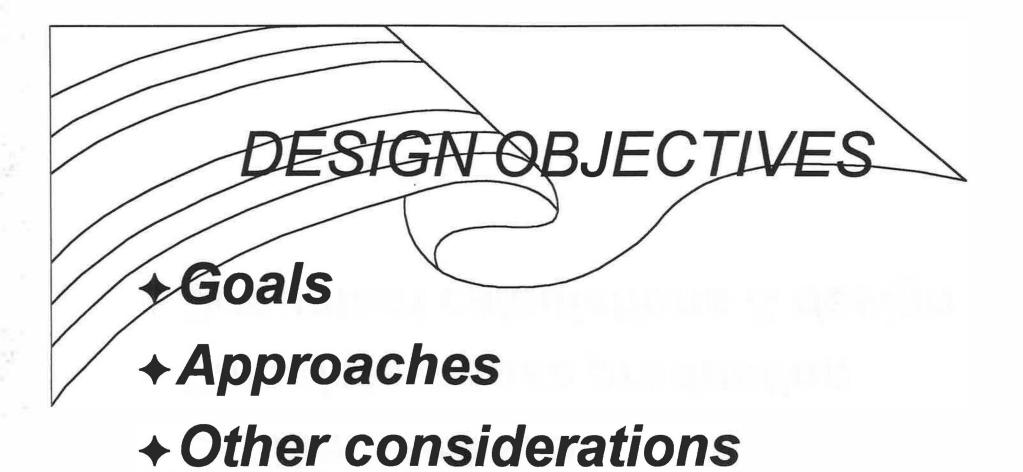






er Effect on Toxicity Combustion products generally allow egress - caution: shielded fires + Temperature below dangerous value + Obscuration is great - visibility potential danger to egress





REDUCE DEATH AND INJURY FROM SMOKE REDUCE PROPERTY DAMAGE FROM SMOKE

ALS

+*AID FIRE FIGHTERS*

*****PROTECT EGRESS PATHS FOR SUFFICIENT TIME TO PERMIT SAFE EVACUATION

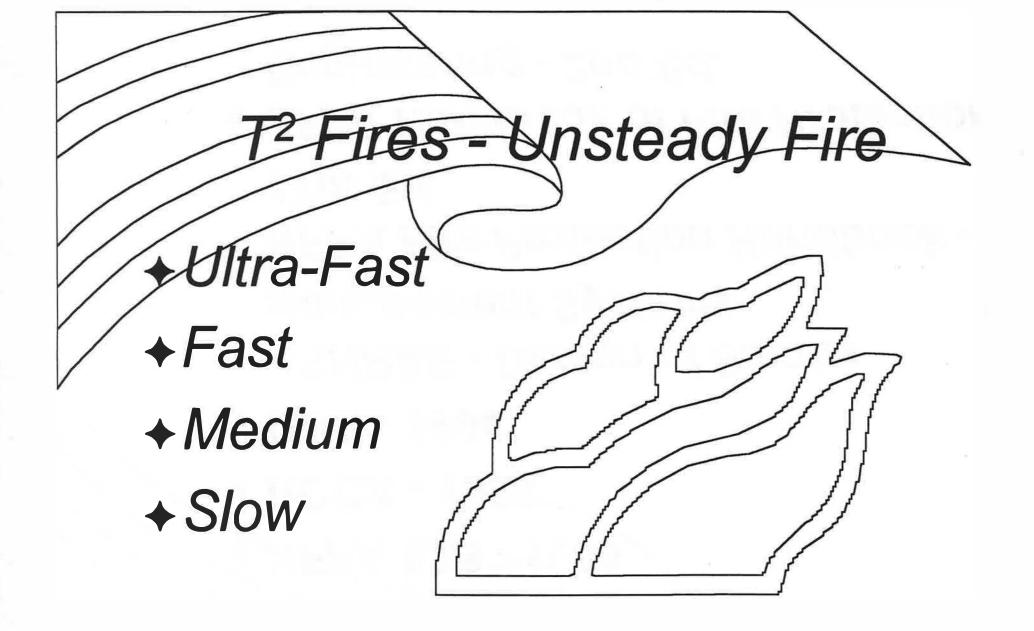
+CONFINE SMOKE TO AREA OF ORIGIN

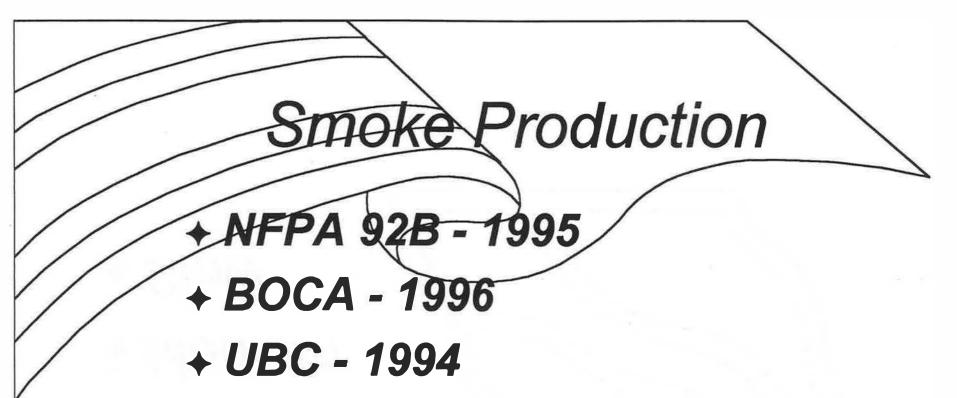
ROACHES

MAINTAIN SMOKE LAYER AT A HEIGHT TO PERMIT FIRE FIGHTERS ACCESS TO REACH SEAT OF THE FIRE

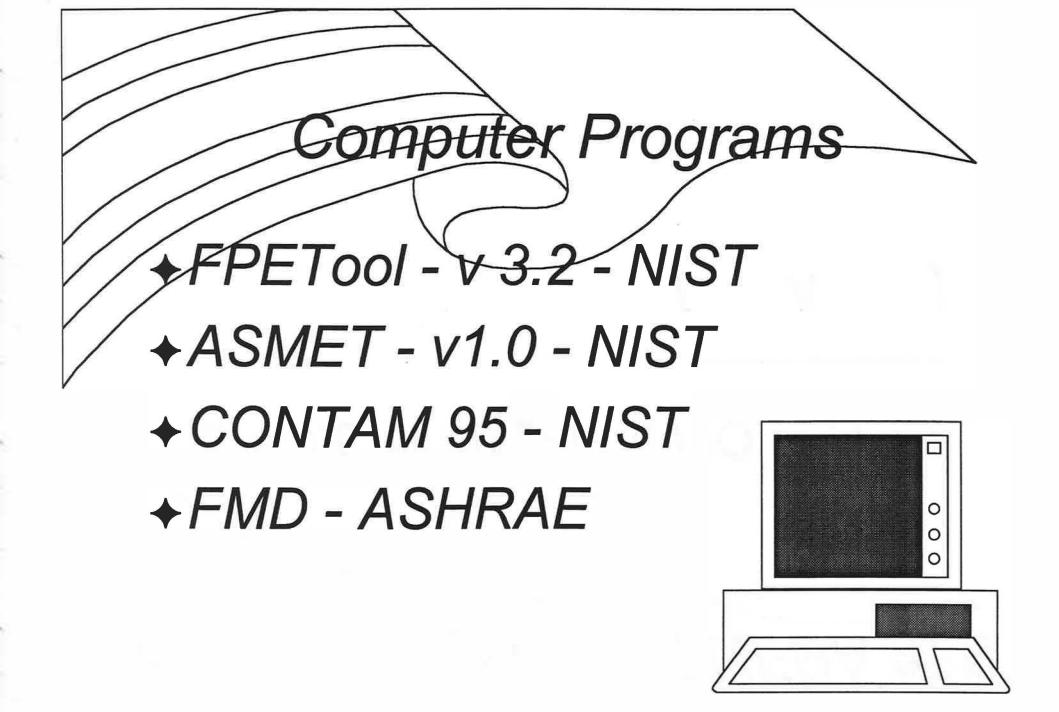
ONSIDERATIONS MINIMIZE COST BY USING **NORMAL HVAC +**MAINTAIN SYSTEM SIMPLICITY TO IMPROVE RELIABILITY





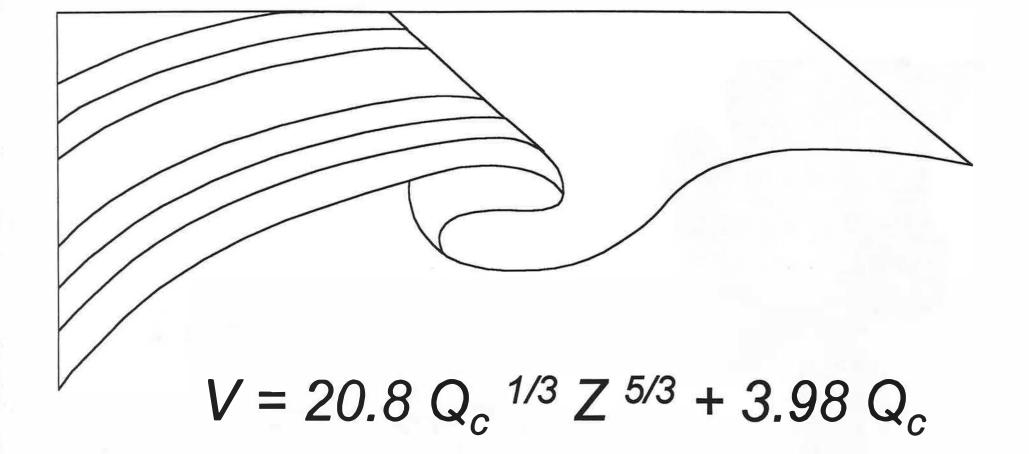


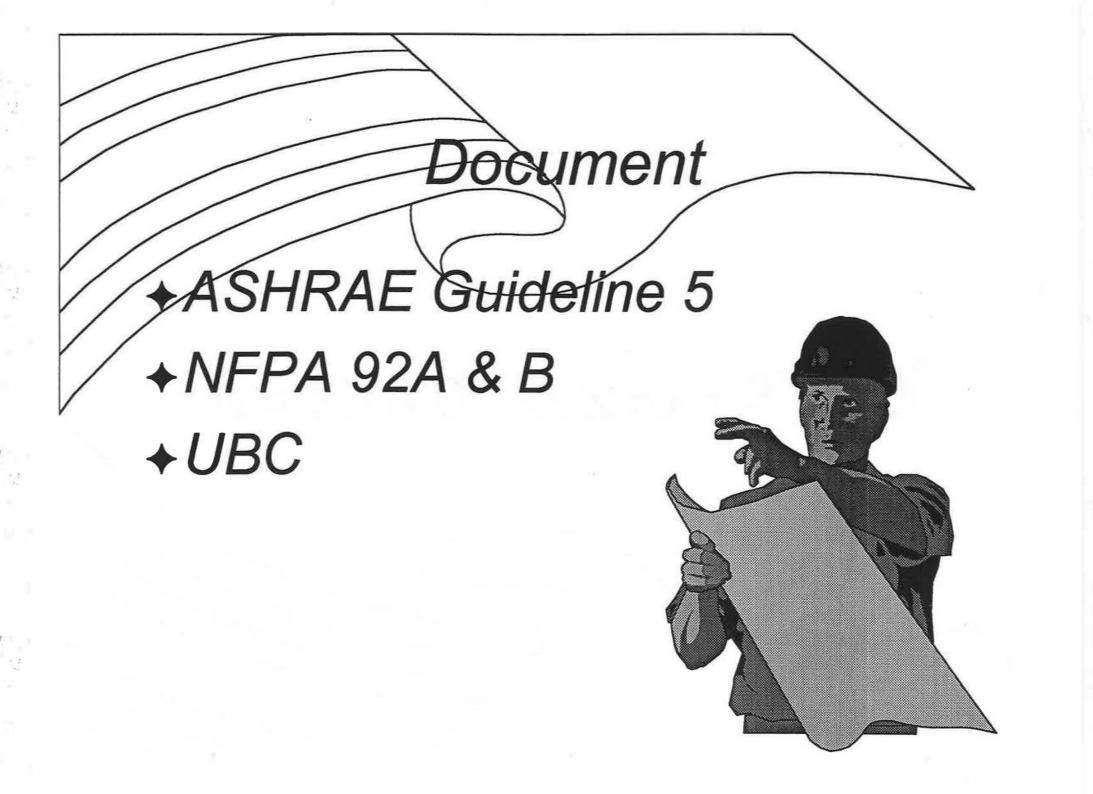
- + ASHRAE Design of Smoke Management Systems
- + NFPA Fire Protection Handbook -17th Ed.
- + SFPE Handbook of Fire Protection Engineering - 2nd Ed.



daptation of NFPA 92B $Z = 0.67H - 0.28H \ln [tQ^{1/3}H^{2/3}]$

Α





+ Research & improved SW & HW + Beware - Fire is unpredictable.

 Calculations are only as good as the underlying research.

Conclusion

– Experience & judgement still needed







